

Speedy Gibbs Sampling for **A^TCA** Equilibrium Systems

M. Neumayer and C. Fox

Institute of Electrical Measurement and Measurement Signal Processing, Inffeldgasse 23/II, A-8010 Graz, Graz University of Technology

8.1.2013



Outline

- Short introduction to inverse Problems
- Introduction to A^TCA systems
- Computational issues
- Fast conditional sampling
- Example on Electrical Capacitance Tomography (ECT)

Inverse Problems

Determine $\boldsymbol{x} \in \mathbb{R}^N$ from

$$\tilde{\boldsymbol{d}} = \boldsymbol{P}(\boldsymbol{x}) + \boldsymbol{v}, \tilde{\boldsymbol{d}}, \boldsymbol{v} \in \mathbb{R}^{M}$$
 (1)

Forward map (model) $F : \mathbf{x} \mapsto \mathbf{y}$.

$$\boldsymbol{y} = \boldsymbol{F}(\boldsymbol{x}) \tag{2}$$

$$F(\mathbf{x}) = P(\mathbf{x}) \quad \forall \mathbf{x},$$
 (3)

Where does the name come from:

$$\boldsymbol{x} = \boldsymbol{F}^{-1}(\tilde{\boldsymbol{d}}), \tag{4}$$

Does not work as inverse problems are ill posed.

Regularization

$$ightarrow \mathscr{F}^{-1}(\widetilde{\boldsymbol{d}})$$

Prior knowledge



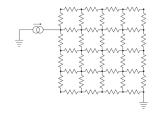
$A^T CA$ what are they? Why are they important?

- What are they: Systems where the underlying stiffness matrix *K* can be expressed by the form *A^TCA*. *C* is diagonal and contains the parameter (material values, etc.). *A* is a mapping.
 - The stiffness matrix depends linear to C
 - The system itself is nonlinear.
- Why are they so important?: The appear in many inverse problems with an underlying electrical, mechanical, heat transfer, hydraulic, etc. problem (Gilbert Strang).
- More general: everything with an underlying resistor network structure → so even in finite element discretiations of pde's.



Resistor Network

$$\boldsymbol{K}_{(l,m)} = \begin{cases} -\frac{1}{R_{(l,m)}} & l \neq m \\ \sum_{k=1}^{N} \frac{1}{R_{(l,k)}} & l = m \end{cases}$$
(5)



 $A^T CA$ decomposition:

$$C_{(l,m)} = \begin{cases} \frac{1}{R_{(l,m)}} & (l,m) \in \mathscr{D} \\ 0 & \text{otherwise} \end{cases}$$
(6)

 $A_{(I,m)} = \begin{cases} +1 & '+' \text{ end of resisor } I \text{ is connected to node } m \\ -1 & '-' \text{ end of resisor } I \text{ is connected to node } m \\ 0 & \text{otherwise} \end{cases}$ (7)



How to obtain a full rank system?

Reduction of the reference node (nodal analysis)

$$\mathbf{Y}\mathbf{u}=\mathbf{i} \tag{8}$$

Most common method in circuit analysis. Easy to implement - just skip the reference column from A.

Penalty method: Add some large number to the reference node. Simple, but not exact, Problem with the condition number.

Variational formulation

$$\boldsymbol{u} = \operatorname{argmin} \boldsymbol{u}^{T} \boldsymbol{K} \boldsymbol{u} - \boldsymbol{i}^{T} \boldsymbol{u}$$
(9)
s.t. $\boldsymbol{u}^{T} \boldsymbol{\chi} = 0$ (10)

$$ightarrow$$
 Constraint optimization problem

*We have not found a better name yet



Non-standard penalty method*

Approach

$$\boldsymbol{u} = \operatorname{argmin} \boldsymbol{u}^T \boldsymbol{K} \boldsymbol{u} - \boldsymbol{i}^T \boldsymbol{u}$$
(11)

$$\mathrm{s.t.}\boldsymbol{u}^{T}\boldsymbol{c}=0 \tag{12}$$

with $\boldsymbol{i}^T \boldsymbol{c} \neq 0$

Unconstraint optimization problem

$$\boldsymbol{u} = \operatorname{argmin}(\boldsymbol{u}^{T}\boldsymbol{K}\boldsymbol{u} - \boldsymbol{i}^{T}\boldsymbol{u}) + \lambda \boldsymbol{u}^{T}\boldsymbol{c}^{T}\boldsymbol{c}\boldsymbol{u}$$
(13)

- Exact method for any value of λ (conditioning), the equation system preserves all nice properties (symmetry, poss. def.).
- i has to contain the input currents and the output current at the reference node!

*We have not found a better name yet



Solution with Green's Functions

- For all further derivations we assume that $\mathbf{K} = \mathbf{A}^T \mathbf{C} \mathbf{A}$ has full rank.
- Our problem

$$\boldsymbol{K}\boldsymbol{u} = \boldsymbol{b} \tag{14}$$

is often a self adjoint (K is symmetric) problem

Solve for Green's functions g

Solve

$$\boldsymbol{K}\boldsymbol{g}_i = \boldsymbol{e}_i, \tag{15}$$

where e_i is the *i*th unit vector

Solution

$$u_i = \boldsymbol{g}^T \boldsymbol{b} \tag{16}$$

Jacobian operation for Ku = b

Lets start with $J: \boldsymbol{C} \mapsto \boldsymbol{u}$

$$(\boldsymbol{K} + d\boldsymbol{K})(\boldsymbol{u} + d\boldsymbol{u}) = \boldsymbol{b}, \qquad (17)$$

can be rearranged to

$$Kdu = -dK(u + du).$$
(18)

$$\frac{d\boldsymbol{u}}{dc_j} = -\boldsymbol{K}^{-1} \frac{d\boldsymbol{K}}{dc_j} \boldsymbol{u}.$$
 (19)

Chain rule

$$d\boldsymbol{u} = \boldsymbol{J}d\boldsymbol{c} = -\sum_{j} \boldsymbol{K}^{-1} \frac{d\boldsymbol{K}}{dc_{j}} \boldsymbol{u}dc_{j} = -\boldsymbol{K}^{-1} \left[\sum_{j} \frac{d\boldsymbol{\hat{K}}}{du_{j}} du_{j} \right] \boldsymbol{u} \quad (20)$$
$$= -\boldsymbol{K}^{-1} \boldsymbol{K}_{d\boldsymbol{c}} \boldsymbol{u}. \quad (21)$$

8.1.2013



The last equation still requires $\hat{\boldsymbol{K}}^{-1} \longrightarrow$ replace by **G**

$$d\boldsymbol{u} = -\boldsymbol{G}^{\mathsf{T}}\boldsymbol{K}_{d\boldsymbol{C}}\boldsymbol{G}.$$
 (22)

Similar $J^T : \mathbf{r} \mapsto \mathbf{C}$

$$\boldsymbol{J}^{T}\boldsymbol{r} = -\text{diag}(\left(\boldsymbol{G}^{T}\boldsymbol{A}^{T}\right)^{T}\left(\boldsymbol{R}\boldsymbol{G}^{T}\boldsymbol{A}\right)), \qquad (23)$$

with $\mathbf{R} = \text{diag}(\mathbf{r})$ We have

- a linear approximation and can do
- gradient based optimization

for free by maintaining Green's functions.



Exact low rank updates for Ku = b

How does *u* change when a low number of elements 0f *C* are updated? Purpose: line search, conditional sampling Woodbury Formula:

$$\left(\boldsymbol{K} + \boldsymbol{U}\boldsymbol{W}^{T}\right)^{-1} = \boldsymbol{K}^{-1} - \underbrace{\boldsymbol{K}^{-1}\boldsymbol{U}\left(\boldsymbol{I} + \boldsymbol{W}^{T}\boldsymbol{K}^{-1}\boldsymbol{U}\right)^{-1}\boldsymbol{W}^{T}\boldsymbol{K}^{-1}}_{\text{update term}}, \quad (24)$$

How can we use this:

$$\boldsymbol{K}_{\text{new}} = \boldsymbol{K}_{\text{old}} + \gamma \boldsymbol{A}^{T} \boldsymbol{C}_{\Delta} \boldsymbol{A}^{T} = \hat{\boldsymbol{K}}_{\text{old}} + \gamma \boldsymbol{U} \boldsymbol{W}^{T}$$
(25)

With ${m G}$ to replace ${m K}_{\rm old}^{-1}$

$$\Delta \boldsymbol{u} = -\gamma \boldsymbol{G}^{\mathsf{T}} \boldsymbol{U} \left(\boldsymbol{I} + \gamma \boldsymbol{W}_{:,C}^{\mathsf{T}} \boldsymbol{G}_{C,C} \boldsymbol{U}_{C,:} \right)^{-1} \boldsymbol{W}^{\mathsf{T}} \boldsymbol{G},$$
(26)

Drawback: $G_{C,C}$ (Green's functions for the effected nodes C) is needed

A ^T CA	8.1.2013			SUQ'13
	イロト 不良 と 不同 と 不同 と	12	DQC	11/34



Woodbury for $\mathbf{A}^T \mathbf{S} \mathbf{A}$ systems 1

Can we do better for our system structure? Assume

$$\boldsymbol{K}_{\text{old}} = \boldsymbol{A}^{T} \boldsymbol{C} \boldsymbol{A}^{T}, \qquad (27)$$

with **S** being a $m \times m$ diagonal matrix and **A** being a $m \times n$ matrix.

$$\boldsymbol{K}_{\text{new}} = \boldsymbol{A}^{T} \boldsymbol{C} \boldsymbol{A} + \boldsymbol{A}^{T} \boldsymbol{C}_{\Delta} \boldsymbol{A}, \qquad (28)$$

With the decomposition: $\boldsymbol{U} = \boldsymbol{A}^T$ and $\boldsymbol{W}^T = \boldsymbol{C} \Delta \boldsymbol{A}$, the Woodbury is given as

$$\boldsymbol{K}_{\text{new}}^{-1} = \boldsymbol{K}_{\text{old}}^{-1} - \boldsymbol{K}_{\text{old}}^{-1} \boldsymbol{A}^{T} \left(\boldsymbol{I} + \boldsymbol{C}_{\Delta} \boldsymbol{A} \boldsymbol{K}_{\text{old}}^{-1} \boldsymbol{A}^{T} \right)^{-1} \boldsymbol{C} \Delta \boldsymbol{A} \boldsymbol{K}_{\text{old}}^{-1}, \qquad (29)$$

Is there a way to replace $\boldsymbol{K}_{\text{old}}^{-1}$?



Woodbury for
$$A^T CA$$
 systems 2

Assume

$$\boldsymbol{K}_{\text{old}}^{-1} = \boldsymbol{J}_1^{-1} \boldsymbol{C}^{-1} \boldsymbol{J}_2^{-T}, \tag{30}$$

Thus

$$\boldsymbol{A}^{T}\boldsymbol{C}\boldsymbol{A}\boldsymbol{J}_{1}^{-1}\boldsymbol{C}^{-1}\boldsymbol{J}_{2}^{-T}=\boldsymbol{I}.$$
(31)

•
$$CC^{-1} = I \dots \checkmark$$

• $A^T J_2^{-T} = I \dots J_2^{-T}$? Pseudo inverse
 $J_2^{-1} = \underbrace{(AA^T)}_{\text{Laplacian}} \overset{-1}{A}$ (32)

•
$$AJ_1^{-1} = I \dots$$
 not possible



Woodbury for $\mathbf{A}^T \mathbf{C} \mathbf{A}$ systems 3

 J_1^{-1} is a problem. However, lets insert it into the inverse of the Woodbury matrix

$$\left(\boldsymbol{I} + \boldsymbol{C}_{\Delta}\boldsymbol{A}\boldsymbol{K}_{\text{old}}^{-1}\boldsymbol{A}^{T}\right)^{-1} = \left(\boldsymbol{I} + \boldsymbol{C}_{\Delta}\boldsymbol{A}\boldsymbol{J}_{1}^{-1}\boldsymbol{C}^{-1}\boldsymbol{J}_{2}^{-T}\boldsymbol{A}^{T}\right)^{-1}, \quad (33)$$

$$= (\mathbf{I} + \mathbf{C}_{\Delta} \mathbf{C}^{-1} \mathbf{J}_2^{-T} \mathbf{A}^T)^{-1}, \qquad (34)$$

- Instead of $G_{C,C}$ now only the diagonal matrix **S** has to be inverted. J_2^{-T} can be computed in advance.
- Again, this form can be reduced and Green's functions can be used on the left and right hand side!



Electrical Capacitance Tomography

- Inverse problem using capacitance measurements.
- Ill-posed → regularization or prior knowledge required.
- Suitable for process tomography due to good contrast of the permittivity (i.e. oil/water).
- Noninvasive.
- Cheap instrumentation but low spatial resolution due to soft field.



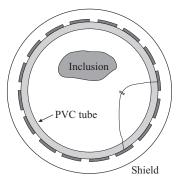
Non ionizing \rightarrow safe.

Neumayer et. al.: Current Reconstruction Algorithms in Electrical Capacitance Tomography, Springer 2010

A ^T CA	8.1.2013			SUQ'13
	・ロット 4 間 > ・ 4 回 > ・ 4 回	•	5 DQC	15/34



Electrical Capacitance tomography



- Ω: whole domain
- Ω_{ROI} : interior of the pipe.
- $\partial \Omega_{ROI}$: interior of the pipe.

PDE:

$$\nabla \cdot (\varepsilon_0 \varepsilon_r \nabla V) = 0, \qquad (35)$$

BC:

$$V_{\partial\Omega} = 0,$$
 (36)

$$V_{\Gamma_i} = V_{\Gamma_i}, \qquad (37)$$

$$V_{\Gamma_j} = 0 \quad \forall j \neq i,$$
 (38)

Gauss law:

$$C_{i,j} = -\frac{1}{V_{\Gamma_i}} \oint_{\Gamma_j} \varepsilon_0 \varepsilon_r \nabla V \cdot \vec{\mathbf{n}} d\Gamma.$$
(39)

Gives a $N_{elec} \times N_{elec}$ matrix.



Standard computations: $F : \varepsilon \mapsto C$

...

8.1.2013

Finite element system:

$$\boldsymbol{K} = \sum_{i=1}^{N_{\boldsymbol{e}}} \varepsilon_i \boldsymbol{K}_{\boldsymbol{e},i}, \tag{40}$$

With BC:

$$\hat{\boldsymbol{K}}\boldsymbol{v}=\boldsymbol{r}.$$

Charge method:

$$Q_{elec} = \sum_{n_{elec}} (\mathbf{K} \mathbf{v})_{n_{elec}}, \qquad (42)$$

Derivatives:

$$dC_{i,j} = \gamma_j^T \left[\left[\frac{\partial \boldsymbol{r}}{\partial \varepsilon_k} \right] - \left[\frac{\partial \hat{\boldsymbol{k}}}{\partial \varepsilon_k} \right] \boldsymbol{v}_i \right] d\varepsilon_k, \tag{43}$$

	4	ð	Þ.	•	Ξ.	×.	•	Ξ.	•	-	5	90	1	7/34



Fast material update

Eigenvector decomposition:

$$\boldsymbol{K}_{\mathrm{e}} = \boldsymbol{V}_{\mathrm{e}} \boldsymbol{D}_{\mathrm{e}} \boldsymbol{V}_{\mathrm{e}}^{-1}, \qquad (44)$$

If
$$\boldsymbol{K}_{e} = \boldsymbol{K}_{e}^{T}$$
:
 $\boldsymbol{K}_{e} = \boldsymbol{A}_{e}^{T} \boldsymbol{S}_{e} \boldsymbol{A}_{e},$ (45)

For FE system

$$\boldsymbol{K} = \boldsymbol{K}_{ini} + \sum_{l=1}^{p} \boldsymbol{A}_{l}^{T} \mathscr{E} \boldsymbol{A}_{l}, \qquad (46)$$

with K_{ini} such that K has full rank (includes the BC).

CA	8.1.2013	SUQ'13
	◆□▶ ◆□▶ ◆臣▶ ◆臣▶ 臣 めんの	18/34



Charge map:
$$Q_c: V_{\partial \Omega_{ROI}} \mapsto \Delta Q$$

How does the potential on the tube influences the charge on the electrodes? Solve

$$\nabla \cdot (\varepsilon_0 \varepsilon_r \nabla V) = 0 \tag{47}$$

in $\Omega \setminus \Omega_{ROI}$ with BC:

$$V_{\partial\Omega} = 0, \qquad (48)$$

$$V_{\partial\Omega_{ROI}} = \delta(\mathbf{x} - \mathbf{x}_i) \qquad \forall \mathbf{x}_i \in \partial\Omega_{ROI}$$
(49)

$$V_{\Gamma_j} = 0 \qquad \forall j, \tag{50}$$

Discrete version $\boldsymbol{Q}_{c}: \boldsymbol{v}_{\partial \Omega_{ROI}} \mapsto \Delta \boldsymbol{Q}$

$$\mathbf{Q} = \mathbf{Q}_a + \mathbf{Q}_c \, \mathbf{V}_{\partial \Omega_{ROI}},\tag{51}$$

 $\textbf{V}_{\partial\Omega_{ROI}}$ contains the nodal potentials on $\partial\Omega_{ROI}$

8.1.2013						SUQ'13
4	< 67 ►	< ≣ >	★目≯	臣	$\mathcal{O}\mathcal{A}\mathcal{O}$	19/34



Solution with Green's functions

$$\hat{\boldsymbol{K}}\boldsymbol{G} = \boldsymbol{E}_{\partial\Omega_{ROI}},\tag{52}$$

$$\boldsymbol{V}_{\partial\Omega_{ROI}} = \boldsymbol{G}^{T} \boldsymbol{R}, \tag{53}$$

R contains the right hand side terms for each electrode.

$$\mathbf{Q} = \mathbf{Q}_a + \mathbf{Q}_c \underbrace{\mathbf{G}^T \mathbf{R}}_{\mathbf{V}_{\partial \Omega_{ROI}}}, \tag{54}$$

... is bad, because $\boldsymbol{E}_{\partial\Omega_{ROI}}$ in equation (52) means the solution for all nodes on $\partial\Omega_{ROI}$. Trick:

$$\hat{\boldsymbol{K}}\boldsymbol{G}\boldsymbol{Q}_{c}^{T} = \boldsymbol{E}_{k}\boldsymbol{Q}_{c}^{T}, \qquad (55)$$

$$\hat{\boldsymbol{K}}\boldsymbol{G}_{Q} = \boldsymbol{E}_{k}\boldsymbol{Q}_{c}^{T} = \boldsymbol{R}_{Q}, \qquad (56)$$

Hence:

$$\boldsymbol{Q} = \boldsymbol{Q}_a + \boldsymbol{G}_Q^T \boldsymbol{R}. \tag{57}$$

A ^T CA	8.1.2013		SUQ'13
	イロン 人間 とくほとくほう	E ∽QQ	20/34



Jacobian operations for ECT

• Linearization: $J : \varepsilon \mapsto Q$

$$d\mathbf{Q} = -\mathbf{G}_{Q}^{T} \hat{\mathbf{K}}_{d\varepsilon} \mathbf{G}_{Q}$$
 (58)

$$d\boldsymbol{Q} = -\boldsymbol{G}_{Q}^{T}\left[\sum_{l}^{p} \boldsymbol{A}_{l}^{T} d\mathscr{E} \boldsymbol{A}_{l}\right] \boldsymbol{G}_{Q}. \tag{59}$$

Gradient: $J^T : \mathbf{Q} \mapsto \varepsilon$

$$\boldsymbol{J}^{T}\boldsymbol{q} = -\text{diag}\left(\left(\sum_{l=1}^{p} \left(\boldsymbol{G}_{Q}^{T}\boldsymbol{A}_{l}^{T}\right)^{T} \left(\boldsymbol{Q}\boldsymbol{G}_{Q}^{T}\boldsymbol{A}_{l}\right)\right)\right), \tag{60}$$

 $A^T C A$



Low Rank updates for ECT

With computation of the additional Green's Functions

$$\Delta \mathbf{Q} = -\gamma \mathbf{G}_{Q}^{\mathsf{T}} \boldsymbol{L} \left(\boldsymbol{I} + \gamma \boldsymbol{U}_{:,C} \mathbf{G}_{C,C} \boldsymbol{L}_{C,:} \right)^{-1} \boldsymbol{U} \mathbf{G}_{Q}, \tag{61}$$

■ **A^TCA** form

$$\Delta \mathbf{Q} = -\mathbf{G}_{Q,C_{2},:}^{T} \mathbf{A}_{1,:,C}^{T} \left(\mathbf{I} + \mathbf{S}_{C} \mathbf{S}_{0,C}^{-1} \mathbf{W}_{3,:,C}^{T} \mathbf{W}_{1,:,C} \right)^{-1} \mathbf{S} \mathbf{W}_{1,:,C}^{T} \mathbf{G}_{Q,C_{2},:},$$
(62)



A speed comparison

t _{mesh1}	t _{mesh2}
ms	ms
96	640
4.8	26
35.5	230
0.039	2
3.3	19
360	> 2000
0.48	3.9
3.3	15.5
3.5	16.3
0.66	4.2
11.6	55.4
2.7	14.1
5.6	18
1.1	3
23.8	66
2.9	8
0.895	17.1
	ms 96 4.8 35.5 0.039 3.3 360 0.48 3.3 3.5 0.66 11.6 2.7 5.6 1.1 23.8 2.9



Fast Deterministic Method

$$\boldsymbol{x}^* = \arg\min_{\boldsymbol{x}} \left\| \boldsymbol{F}(\boldsymbol{x}) - \tilde{\boldsymbol{d}} \right\|_2^2 + \alpha \boldsymbol{x}^T \boldsymbol{L}^T \boldsymbol{L} \boldsymbol{x}, \tag{63}$$

Gauss Newton method:

$$\boldsymbol{x}_{k+1} = \boldsymbol{x}_k - \boldsymbol{s} \left(\boldsymbol{J}^T \boldsymbol{J} + \boldsymbol{\alpha} \boldsymbol{L}^T \boldsymbol{L} \right)^{-1} \left(\boldsymbol{J}^T \boldsymbol{r}_k + \boldsymbol{L}^T \boldsymbol{L} \boldsymbol{x}_k \right),$$
(64)

BFGS scheme:

- Evaluate the Newton direction $\boldsymbol{p}_k = -\boldsymbol{H}_k^{-1}\boldsymbol{g}_k$
- 2 Find s to set $\mathbf{x}_{k+1} = \mathbf{x}_k + s\mathbf{p}_k$ and set $\mathbf{s}_k = s\mathbf{p}_k$

3 Compute
$$\boldsymbol{y}_k = \boldsymbol{g}(\boldsymbol{x}_{k+1}) - \boldsymbol{g}(\boldsymbol{x}_k)$$
.

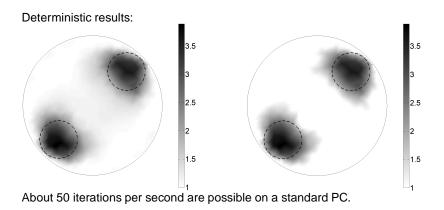
4 Evaluate
$$\boldsymbol{H}_{k+1}^{-1} = \boldsymbol{H}_{k}^{-1} + \frac{\boldsymbol{s}_{k}^{\mathsf{T}}\boldsymbol{y}_{k} + \boldsymbol{y}_{k}^{\mathsf{T}}\boldsymbol{H}_{k}^{-1}\boldsymbol{y}_{k}}{(\boldsymbol{s}_{k}^{\mathsf{T}}\boldsymbol{y}_{k})^{2}}\boldsymbol{s}_{k}\boldsymbol{s}_{k}^{\mathsf{T}} - \frac{\boldsymbol{H}_{k}^{-1}\boldsymbol{y}_{k}\boldsymbol{s}_{k}^{\mathsf{T}} + \boldsymbol{s}_{k}\boldsymbol{y}_{k}^{\mathsf{T}}\boldsymbol{H}_{k}^{-1}}{(\boldsymbol{s}_{k}^{\mathsf{T}}\boldsymbol{y}_{k})^{2}}.$$

8.1.2013

Q C 24/34



Bayesian Inversion



A ^T CA	8.1.2013	SUQ'13
	◆□▶ ◆□▶ ★目▶ ★目▶ 目 のへの	25/34



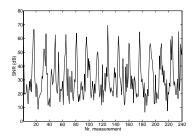
Bayesian Inversion

Posterior to sample from

$$\pi(\boldsymbol{x}|\tilde{\boldsymbol{d}}) \propto \exp\left(-\frac{1}{2}\boldsymbol{e}^{T}\boldsymbol{\Sigma}_{\boldsymbol{v}}^{-1}\boldsymbol{e}\right) \exp\left(-\frac{1}{2}\alpha\boldsymbol{x}^{T}\boldsymbol{L}^{T}\boldsymbol{L}\boldsymbol{x}\right) I(\boldsymbol{x}).$$
(65)

L: smoothing prior

Signal disturbed by additive Gaussian noise.





How to implement a Gibbs sampler

General Steps

- 1 Draw a conditional sample.
- If the new sample is accepted, compute the new forward map to obtain the new Green's functions G_Q for the cheap evaluation of the next conditional sample.

Versions:

- Bimodal (two valued) material distributions
- General material values



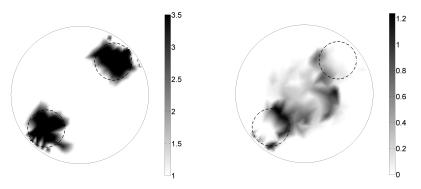
Bimodal Material Distributions

Computation steps:

- 1 Flip one element of \boldsymbol{x} to generate the proposal \boldsymbol{x}' .
- **2** Compute the likelihood ratio $\alpha = \min \left[1, \frac{\pi(\mathbf{x}'|\tilde{\mathbf{a}})}{\pi(\mathbf{x}|\tilde{\mathbf{a}})}\right]$.
- 3 Accept \mathbf{x}' with probability α .



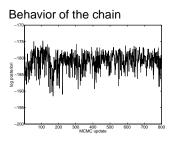
Bimodal Material Distributions

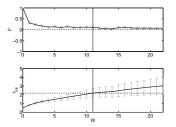


- Mean estimate and standard deviation
- About 3 frames per second are possible using the Jacobian operations



Bimodal Material Distributions

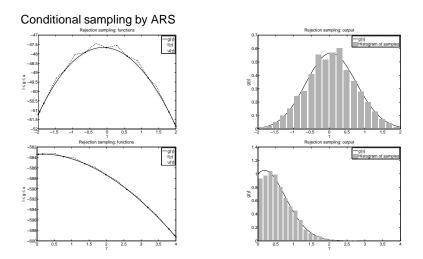




8.1.2013						SUQ'13
• • •	< 67 ►	< ≣ >	★目→	12	DQC	30/34

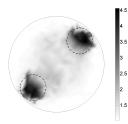


General Gibbs Sampler

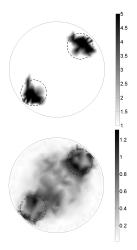




Gibbs Sampler

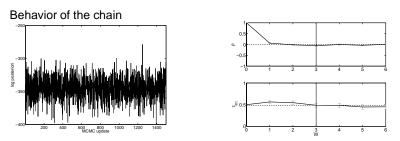


We use a reduced version of ARS - not the correct statistic (can be worked out), but fast. A sample in the time of an optimization result!





Gibbs Sampler



And this is just the most trivial version of a Gibbs sampler!



Summary

- Inverse problems
- General introduction to **A^TCA** systems
- Computational aspects
- Fast low rank updates
- Example on ECT

 \rightarrow with some tricks we can generate samples in the time of an optimization run.

Neumayer and Fox, JUQ 2013