

1       **Observed effects of the May 2024 Gannon Storm on the New Zealand gas pipeline**  
2       **network – towards predicting the effects of an extreme storm**

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9       **Key Points:**

- 10       • Cathodic protection monitoring data from 33 locations on the New Zealand gas pipeline  
11       network during the Gannon Storm are discussed.
- 12       • Major variations in pipe to soil potentials were observed at a number of sites taking the  
13       potential outside the desired protection range.
- 14       • Analysis of these variations suggests approaches to modeling the likely effect of extreme  
15       geomagnetic storms on the network.  
16

**17 Abstract**

18 We present cathodic protection monitoring data from the New Zealand gas pipeline network  
19 during the Gannon Storm of May 2024. At some locations potentials between the pipe and a  
20 Cu/CuSO<sub>4</sub> reference cell and between an installed metal coupon and the reference cell both  
21 underwent large variations - changes which took the pipeline outside the desired potential  
22 range for cathodic protection. At these locations both potentials became positive for significant  
23 lengths of time, which, in the event of defects in the pipe coating, can lead to corrosion of the  
24 pipe. Highly negative pipe to reference cell potentials, which can lead to detachment of the  
25 coating from the pipe, were also observed. Pipe to reference cell potentials and coupon to  
26 reference cell potentials are both indicators of the level of cathodic protection. The observed  
27 relationship between them when the rectifier is turned off are seen to have a complex form.  
28 Whilst the relationship is linear over a reasonably wide range of pipe to reference cell  
29 potentials, coupon-off potentials at some sites approach an asymptotic limit at highly negative  
30 pipe potentials, but rise sharply and become scattered at larger, including positive, pipe  
31 potentials. At locations where pipe to reference cell potentials are not routinely monitored,  
32 measurements of the potential between the anode bed and the pipe may be used to assess the  
33 level of cathodic protection. Assessment of the effects of the Gannon Storm allow the  
34 development of methods of predicting the effect of extreme storms on the network, which we  
35 put forward here.

36

**37 Plain Language Summary**

38 Variations in Earth's magnetic field during geomagnetic storms induce electric currents  
39 (geomagnetically induced currents) in the ground which, in certain circumstances, may disrupt  
40 the cathodic protection systems used to protect buried gas pipelines from corrosion. In this  
41 study we report the response of the New Zealand gas pipeline network to the Gannon Storm of  
42 May 2024, the largest geomagnetic storm for approximately 20 years. Studying and  
43 understanding the response of the pipeline network to this storm is important in developing  
44 methods to predict the likely response to extreme geomagnetic storms which may be up to 10  
45 times larger and may present a risk to the integrity of the network.

## 46 **1 Introduction**

47 Geomagnetically induced currents present a potential risk to the cathodic protection  
48 (CP) systems (Gummow, 2002) that protect long pipelines from corrosion. Since the Effects on  
49 the Alaska pipeline were first recognized and investigated by Gideon (1971) and Campbell  
50 (1978, 1980), further studies have been conducted on pipelines in Argentina (Osella et al.,  
51 1998), Australia (Marshall et al., 2010, 2013), Canada (Fernberg et al., 2007), and Finland (Hajra,  
52 2022; Pirjola et al., 2003; Pulkkinen et al., 2001; Viljanen, 1989; Viljanen et al., 2006, 2010).  
53 Studies have also been undertaken in New Zealand, as detailed below.

54 The effects of geomagnetically induced currents (GIC) on the New Zealand gas pipeline  
55 network have previously been discussed by Ingham et al. (2022) and Divett et al. (2023).  
56 Ingham et al. (2022) presented examples of monitoring data from 10 locations on the network  
57 and discussed the possible implications of GIC for the cathodic protection (CP) system that  
58 protects the pipeline. Divett et al. (2023) subsequently presented first attempts at modeling  
59 pipe to soil potentials on the New Zealand pipeline. Although the results of both studies were  
60 illuminating in showing the response of the pipeline network to geomagnetic activity, the  
61 magnetic storms used in the studies (Ingham et al. 2022, Table 1) were from the declining  
62 phase of Solar Cycle 24 and were of relatively small size, with only one storm reaching a  $Kp$   
63 max of 7+. In contrast, the magnetic storm of 10-13 May 2024, the Gannon Storm, had a  $Kp$   
64 max of 9- to 9 and the response of the pipeline network to this significantly larger storm may  
65 provide a more reliable guide to the potential impact of an extreme storm on the CP system.

66 In this paper we therefore present and discuss the observed effects of the Gannon  
67 Storm of May 2024 on the New Zealand pipeline network based on monitoring data from 33  
68 locations across the network. We start with a review of the pipeline network, its CP system, and  
69 the parameters which are monitored. We then look, in turn, at specific aspects of the observed  
70 response of the pipeline to the storm and discuss approaches to predicting the likely effect of  
71 extreme geomagnetic activity on the network. Our industry partners are interested in the  
72 possible impact of extreme geomagnetic disturbances such as the Carrington event of 1859  
73 (Carrington, 1859; Tsurutani, 2003), so they can quantify the risk to their infrastructure and  
74 systems. Such impacts extend from damage to aspects of the physical infrastructure to the  
75 possibility of enhanced corrosion at any defect in the pipe coating. Although we deal with the  
76 New Zealand pipeline network it is hoped that many of the conclusions will be relevant to  
77 pipeline networks in other countries.

## 78 **2 The New Zealand gas pipeline network and CP system**

79 The New Zealand gas pipeline network and the monitoring sites used in this paper are  
80 shown in Figure 1. As discussed by Ingham et al. (2022), and shown schematically in Figure 2,  
81 the CP system consists of a constant current rectifier at each of the sites, which applies a  
82 potential difference between an anode bed and the pipe such that the pipe is negative with  
83 respect to the adjacent ground. Both the rectifier output current and what Ingham et al. (2022)  
84 referred to as the “rectifier output voltage” are measured at each site with 1 s time resolution.

85 Also monitored at 1 second sampling at some rectifier sites are two other quantities.  
86 One of these is the potential difference between the pipe and a Cu/CuSO<sub>4</sub> reference cell near to

87 the pipe. In the current study we refer to this potential difference as the pipe to soil potential  
 88 (*PSP*). At a further reduced number of sites a metal coupon is installed adjacent to the pipe and  
 89 the potential difference between this and the reference cell (the coupon potential) is  
 90 monitored. As explained by Gummow (2002) the pipe to reference cell potential is made up of  
 91 two parts – the polarization potential between the pipe and the adjacent ground due to  
 92 electrochemical effects, and the potential drop through the ground between the pipe and the  
 93 reference electrode. This latter part is itself made up of two factors – the potential drop  
 94 through the ground due to the cathodic protection current supplied by the rectifier and a time  
 95 varying component resulting from the presence of GIC. This may be represented as

$$96 \quad PSP = V_p + IR \pm V_{GIC} \quad (1)$$

97 where  $V_p$  is the polarization potential between the pipe and the adjacent ground,  $IR$  is the  
 98 potential drop through the ground due to the cathodic protection current, and  $V_{GIC}$  is the  
 99 contribution to the *PSP* due to geomagnetically induced current. When the rectifier is turned  
 100 off the second term on the right-hand side of equation (1) is removed and the *PSP*, within the  
 101 limits of any  $V_{GIC}$ , gives an estimate of the polarization potential. Here, we refer to the pipe to  
 102 soil potential when the rectifier is turned on as *PSP-on*, and that when the rectifier is turned off  
 103 as *PSP-off*.

104 To obtain an estimate of the polarization potential that does not include the effect of  
 105  $V_{GIC}$ , a metal coupon is installed close to the pipe surface. This simulates a defect in the pipeline  
 106 coating. As explained by Gummow (2002), and shown in Figure 1 of Ingham et al. (2022), it is  
 107 connected to the pipe through a test station and the reference electrode is installed close to  
 108 the coupon. Thus, when the rectifier is turned off the effects of both the cathodic protection  
 109 current and GIC in equation (1) are removed, and the potential difference between the coupon  
 110 and the reference electrode gives a measure of the polarization potential between the pipe and  
 111 the ground. It is this potential difference between the coupon and the reference cell when the  
 112 rectifier is turned off, referred to here as the “coupon-off” potential, which is regarded as the  
 113 best measure of the polarization potential. The accepted industry standard is that the coupon-  
 114 off potential should be in the range -0.85 V to -1.2 V to ensure that the pipe is protected (Popov  
 115 & Lee, 2018). Polarization potentials higher than -0.85 V may expose the pipe to enhanced  
 116 corrosion, while potentials significantly lower than -1.2 V may result in “disbonding” where the  
 117 pipe coating becomes detached from the pipe (Ingham et al., 2022). Ackland & Dylejko (2019)  
 118 discussed in detail the electrochemical reactions that take place at a pipe surface and how  
 119 accurate a measure of the true polarization potential the coupon-off potential actually is. They  
 120 concluded that the coupon-off potential (the “instant off potential” in their terminology) is  
 121 always slightly more positive than the true polarization potential and represents the corrosion  
 122 potential at the time of rectifier turn off – essentially a measure of the propensity of the pipe to  
 123 oxidise in the environment to which it is exposed.

124 On the New Zealand pipeline network the interval between times when the rectifier is  
 125 turned off varies from rectifier to rectifier, being only 5 or 10 minutes at some locations but up  
 126 to 6 hours at others. At each turn off the rectifier is off for 3 seconds. The rectifiers on the New  
 127 Zealand gas pipelines are normally set to give a constant current output, that is, the rectifier  
 128 varies the output voltage to keep the protection current at a constant level, within set limits of

129 the rectifier. As has been previously observed (Ingham et al., 2022) in general the current  
130 changes only slightly and this typically happens when there are rapid variations in the Earth's  
131 magnetic field, i.e., during significant space weather events. The rectifier voltage itself has a  
132 restricted range and the monitored "rectifier output voltage", like the pipe to reference cell  
133 potential, contains a time varying component due to GIC. It can therefore be more correctly  
134 identified as the total potential difference between the anode bed, through which the  
135 protection current is injected (Figure 2), and the pipe. It is the summation of the actual rectifier  
136 output voltage and the potential due to GIC passing onto and off the pipe. We subsequently  
137 refer to this as the anode bed to pipe potential (*APP*). The rectifier output voltage is controlled  
138 by pulse width modulation on a 38 Hz cycle, with the voltage set to achieve the necessary  
139 constant-current that keeps the pipe sufficiently negative with respect to ground with a 75% on  
140 pulse width modulation. Thus, an induced potential due to GIC of  $\sim 1.3x$  the 'normal' output  
141 voltage, will match the rectifier supply voltage and will drop the output current to zero, or in  
142 some instances possibly even reverse it. In this paper we draw distinction between the limited  
143 rectifier output voltage and the effect of GIC on *APP*.

### 144 **3 The geomagnetic storm of 10-13 May 2024**

145 The geomagnetic storm of 10-13 May 2024 was the largest event since at least the  
146 Halloween Storm of 2003, with a *Kp* index between 8- and 9 and these disturbance levels were  
147 sustained for a full 33 hours. As such it provides an excellent opportunity to investigate the  
148 impact that major geomagnetic activity has on the cathodic protection (CP) system on the New  
149 Zealand gas pipeline network. The magnetic field variations in the 1-second sampled northward  
150 ( $B_x$ ) and eastward ( $B_y$ ) components of the magnetic field as recorded over 10-13 May 2024 at  
151 the Eyrewell geomagnetic observatory, near Christchurch in New Zealand's South Island, are  
152 shown in Figure 3. Also shown in Figure 3 are the rates of change (in nT/min) of the two  
153 components. The storm commenced with a small increase in  $B_x$  at 1705 on 10 May with major  
154 variations of 100's of nT in both components occurring through until 0534 UT on 12 May. There  
155 was then a further burst of reduced activity starting at approximately 2100 UT on 12 May.

156 The maximum rates of increase of  $B_x$  and  $B_y$  were 360 and 192 nT/min respectively. The  
157 former occurred at 0846 UT on 11 May and was followed about 3 minutes later by the  
158 maximum rate of decrease of -191 nT/min. The maximum rate of increase in  $B_y$  occurred  
159 another 2 minutes later at 0851 UT, and was followed by a maximum rate of decrease in  $B_y$  of -  
160 164 nT/min some 5 minutes after this. These features are clearly seen as the prominent upward  
161 and downward spikes in the  $dB/dt$  panels in Figure 3. In comparison the maximum rates of  
162 change in  $B_x$  and  $B_y$  at Eyrewell during the largest storm studied by Ingham et al. (2022) were  
163 at least a factor of 10 smaller. As the Eyrewell observatory is approximately 300 km south of  
164 Wellington and 750 km south of Auckland it is likely, as was observed for the storm of 17 March  
165 2015, discussed by Divett et al. (2020), that both the magnitude and rate of change of magnetic  
166 field across the pipeline network on 10-13 May 2024 were smaller than these observed values  
167 at Eyrewell. Nevertheless the Gannon storm represents the most significant observed  
168 geomagnetic activity in recent years, and, as stated above, gives the opportunity to assess both  
169 the impact of major activity on the pipeline network, and to allow progress to predicting the  
170 possible effects of an "extreme" storm.

#### 171 4 Pipe to reference cell potential variations during the Gannon Storm

172 Pipe to soil potential (*PSP*) during geomagnetic activity can be calculated theoretically  
 173 using the the equivalent-pi transmission line representation of a pipeline network as shown by  
 174 Boteler (2013). This method has been used for preliminary calculations for the New Zealand  
 175 pipeline network by Divett et al. (2023). It is pertinent therefore to review how the *PSP* at  
 176 monitoring sites behaved during the Gannon Storm. This will go some way to giving insight into  
 177 the likely “extreme” storm response. As reported by Ingham & Rodger (2018) on an earlier  
 178 investigation at a single location in the New Zealand pipe network, when variations due to GIC  
 179 cause the *PSP* to become positive, in the event of a defect in the pipeline coating, a corrosive  
 180 current can pass from the pipe to the ground. Gummow (2002) summarized corrosion theory  
 181 and calculated that, for a 1 cm<sup>2</sup> circular hole in a 0.3 mm thick modern pipeline coating, if the  
 182 surrounding soil has a resistivity of 1000 Ωm the resulting current density due to a potential  
 183 change of 1 V would be 2.5 mA/cm<sup>2</sup>. This was calculated by the authors to give a corrosion rate  
 184 of about 31.3 mm/year for a direct current. Allowing for a change in potential of  $\Delta V$ , the  
 185 dependence of corrosion rate on the period of the variation in potential, and the fraction of  
 186 time ( $t$ ) in a year that the change exists, the overall corrosion rate ( $R$ ) in mm/year was  
 187 expressed as

$$188 \quad R = 31.3 \Delta V t f \quad (2)$$

189 where the factor  $f$  expresses the percentage effect of an alternating current compared to a  
 190 direct current. It depends upon the period of the variation ( $T$ ) in hours and, based on Figure 2 of  
 191 Gummow (2002), may be expressed as

$$192 \quad \log_{10} f \approx 0.18(\log_{10} T + 8.1) \quad (3)$$

193 The authors thus calculated that a 0.5 V shift in potential could cause between 0.06 and 0.152  
 194 mm of corrosion per year depending on the period of the variation.

195 During the Gannon storm *PSP* were measured every second at 16 of the locations shown  
 196 in Figure 1. Shown in Figure 4 are measured *PSP* at Salle Road (SR) over the 96 hours from 0000  
 197 UT on 10 May 2024 . It is apparent from Figure 4 that there were large variations in the  
 198 measured *PSP* and values actually became positive for a substantial amount of the time. As  
 199 outlined above, however, it is the *PSP* when the rectifier is turned off that is of most interest in  
 200 assessing CP, and also the quantity which most closely aligns with *PSP* calculated using  
 201 numerical modelling. Although measurements with the rectifier turned off are much less  
 202 frequent than the 1 second basic sampling interval, if the *PSP* at each turn-off (*PSP-off*) is  
 203 plotted against the potential immediately before turn-off (*PSP-on*) there is observed to be a  
 204 very close relationship between the two quantities. It is observed that at all of the monitoring  
 205 sites this relationship can be expressed as quadratic, as shown for example in Figure 5 for  
 206 measurements at Salle Road. Applying this relationship to all the measured *PSP* at Salle Road  
 207 allows the rectifier off *PSP* (*PSP-off*) to be calculated at the 1 second sampling rate.

208 Listed in Table 1, for the 48 hour period between 1200 UT 10 May 2024 to 1200 UT 12  
 209 May 2024, are the mean, maximum and minimum values of *PSP-off* at these 16 locations,  
 210 calculated as described above, for the rectifier being turned off. Also listed is the cumulative  
 211 lengths of time for which, at each location, *PSP-off* was positive and also the length of time  
 212 when this quantity was less than -2 V. The variations in *PSP-off* over this time period for 8 of the  
 213 sites where values were positive or less than -2 V for significant periods of time are shown in  
 214 Figure 6. Maximum and minimum values that exceeded these values are shown in red in Table  
 215 1, and these limits are marked by the horizontal dashed lines in Figure 6.

216 As can be seen from Table 1 and Figure 6 the largest variations in *PSP-off*, with a range  
 217 of over 12 V, occurred at Salle Road (SR), Waipu Cove Road (WCR) and Raukawa Road (RR).  
 218 Salle Road and Waipu Cove Road are both at the northern end of the pipeline section which  
 219 runs from Auckland to Whangarei (Figure 1), while Raukawa Road is towards the northeastern  
 220 end of the line that runs to Hawkes Bay. These are the same three sites identified by Ingham et  
 221 al. (2022) as being most susceptible to the effects of GIC. At these sites the *PSP-off* was positive  
 222 for a significant part of the 48 hour period – nearly 20% of the time. There were also significant  
 223 periods of positive *PSP-off* at Amriens Road (AR), Queen Elizabeth Park (QEP) and Waimana

| Site | 1200 UT 10 May 2024 – 1200 UT 12 May 2024 |                           |                           |                    |                     |
|------|---|---------------------------|---------------------------|--------------------|---------------------|
|      | Mean <i>PSP-off</i><br>(V)                | Max <i>PSP-off</i><br>(V) | Min <i>PSP-off</i><br>(V) | t > 0 V<br>(h:m:s) | t < -2 V<br>(h:m:s) |
| SR   | -1.162                                    | 4.812                     | -11.400                   | 8:48:03            | 7:22:02             |
| WCR  | -0.903                                    | 8.104                     | -13.813                   | 8:35:25            | 7:12:39             |
| KHR  | -0.910                                    | -0.011                    | -1.654                    | -                  | -                   |
| AR   | -1.032                                    | 3.663                     | -4.268                    | 2:12:37            | 3:37:43             |
| MOH  | -0.966                                    | -0.100                    | -1.785                    | -                  | -                   |
| PR   | -0.937                                    | -0.242                    | -2.287                    | -                  | 0:02:04             |
| DR   | -0.841                                    | -0.625                    | -1.209                    | -                  | -                   |
| TPY  | -0.616                                    | -0.558                    | -0.78                     | -                  | -                   |
| QEP  | -0.907                                    | 2.859                     | -4.766                    | 3:14:59            | 3:10:38             |
| TakR | -1.021                                    | 1.517                     | -4.890                    | 1:44:59            | 1:26:23             |
| JHR  | -0.946                                    | -0.397                    | -2.103                    | -                  | 0:00:14             |
| TB   | 0.306                                     | 3.038                     | -3.633                    | 41:28:14           | 0:07:12             |
| WaR  | -1.230                                    | 4.472                     | -8.423                    | 3:47:09            | 8:00:22             |
| WhR  | -1.169                                    | 0.017                     | -2.541                    | 0:00:02            | 0:11:14             |
| WtR  | -0.735                                    | 0.577                     | -2.190                    | 1:02:08            | 0:01:00             |
| RR   | -1.107                                    | 3.058                     | -9.039                    | 8:29:22            | 7:45:34             |

Table 1: Mean, maximum and minimum values of pipe to reference cell potential calculated from the measured data for the when the rectifier is turned off. The period covered is from 1200 UT 10 May 2024 to 1200 UT 12 May 2024. Also listed are the cumulative lengths of time for which the calculated potential was positive and the cumulative lengths of time for which it was less than -2 V. Extreme values of *PSP* are marked in red.

224 Road (WaR). Of all the sites listed in Table 1, Tumunui Block (TB) stands out as having a mean  
225 value of *PSP-off* which is positive. This is vastly different from any other site and is highly  
226 anomalous. Although it is a situation which would normally indicate a high likelihood of  
227 corrosion, it has existed at Tumunui Block more or less since the rectifier was first installed  
228 nearly 50 years ago and no corrosion has been detected. This anomalous situation probably  
229 results from the locally complex volcanic and geothermal geology of an area which is also laced  
230 with a multitude of south-west to north-east trending faults.

231 The principal times at which the potential became positive at Salle Road, Waipu Cove  
232 Road and Raukawa Road were during the initial phase of the storm, and the periods for which  
233 the potential was continuously positive were several hours long. However, this was not the case  
234 at Amriens Road, Queen Elizabeth Park and Waimana Road. At these locations *PSP* became  
235 positive at different times and for much shorter periods. This difference results from the fact  
236 that the phase of GIC induced variations depends upon where on a segment of pipeline a site is  
237 located (Boteler and Seager, 1998; Ingham et al., 2022; Divett et al., 2023). Thus, at Salle Road  
238 and Waipu Cove Road, at the northern end of the section of pipeline from Auckland to  
239 Whangarei, rises in *PSP* were simultaneous with decreases in *PSP* at Amriens Road, which is at  
240 the southern end of this section of pipeline. Similarly, rises in potential at Queen Elizabeth Park  
241 were coincident with decreases in potential at Takapu Road (TakR) even though both locations  
242 are close to the southern end of the pipeline from Taranaki to Wellington. Thus, at Amriens  
243 Road, Queen Elizabeth Park and Waimana Road the instances of increased *PSP* were  
244 simultaneous with decreases at Salle Road, Waipu Cove Road and Raukawa Road, and typically  
245 were of much shorter duration.

246 As indicated by Ingham et al. (2022), and discussed in detail by Heim & Schwenk (1997),  
247 apart from the issue of corrosion resulting from positive potentials, extremely negative  
248 potentials carry the risk of the pipe coating becoming detached from the pipe, so called  
249 disbonding. Also shown in Table 1 are the lengths of time for which, at each site, the *PSP* was  
250 lower than -2 V. Although the value of -2 V is somewhat arbitrary, it is apparent that almost all  
251 the same sites which show positive *PSP-off* potentials are those that show highly negative  
252 values. Thus, sites susceptible to large variations in *PSP* are potentially at risk both of corrosion  
253 and of disbonding. Potentials less than -2 V also occurred at Salle Road, Waipu Cove Road and  
254 Raukawa Road for significant lengths of time, although the longest length of time for which  
255 potentials were less than -2 V was at Waimana Road. As for the positive *PSP-off* potentials at  
256 Salle Road, Waipu Cove Road and Raukawa Road, this was during the initial phase of the storm  
257 and resulted in long periods of the potential being continuously lower than -2 V. Significant  
258 periods of very negative potentials also occurred at Amriens Road, Queen Elizabeth Park and  
259 Takapu Road.

260 Equation (2) suggests the possibility of a rough calculation of the effective corrosion rate  
261 due to the Gannon Storm. Although the maximum values of potential listed in Table 1 were  
262 significantly higher, the average value of positive potential at Salle Road and Raukawa Road  
263 were slightly less than 1 V, with the corresponding value at Waipu Cove Road being about 1.5 V  
264 – rises in potential from the mean values of about 2.5 V. Also relevant is the typical period  $T$  of



265 the variation in potential which gives rise to positive values. At these three locations, as noted  
 266 above, the dominant period of this variation, at least in the early part of the Gannon Storm, is  
 267 about 3 hours. Thus, taking  $\Delta V \approx 2.5$  V, a value of  $f$  of approximately 0.35 (expressed as a  
 268 percentage, calculated from the period of 3 hours using equation (3)), and taking the 48 hours  
 269 of the storm shown in Figure 6 as 0.0055 of a year, leads to a calculated corrosion rate of 0.151  
 270 mm/year. This represents a first order estimate of the rate calculated from the effect of a single  
 271 storm of  $K_p$  between 8 and 9 and is close to the maximum value quoted by Gummow (2002) for  
 272 the cumulative effect of multiple smaller storms.

## 273 **5 Coupon-off potential variations during the Gannon Storm**

274 Notwithstanding the discussion of the variations in *PSP* when the rectifier is turned off,  
 275 as indicated previously, the industry standard for deeming if a pipe is protected comes from the  
 276 potential between an installed coupon and a Cu/CuSO<sub>4</sub> reference cell, also when the rectifier is  
 277 turned off. Shown in Figure 7 are *coupon-off* measurements from 6 sites during the most  
 278 intense period of geomagnetic activity from 1200 UT 10 May 2024 to 1200 UT 12 May 2024.  
 279 Measurements at Salle Road, Waipu Cove Road and Amriens Road were made every 5 minutes,  
 280 whilst at the other three sites the interval between measurements was 10 minutes. Also shown  
 281 are the -0.85 V and -1.2 V limits that it is recommended that the potential should be between.  
 282 Table 2 lists the mean, maximum and minimum values of the *coupon-off* potentials at all sites  
 283 where it was measured for the 96 hours from 0000 10 May 2024 to 0000 14 May 2024 UT.

284 As can be seen from Figure 7, rises in *coupon-off* potential above the recommended  
 285 upper limit of -0.85 V occurred at all of the sites shown. At Waipu Cove Road, Queen Elizabeth  
 286 Park and Waimana Road the *coupon-off* potential actually became positive at times. As for *PSP-*  
 287 *off*, the timing of such instances was not coincident at each site. This is best evidenced by the  
 288 differences between Waipu Cove Road and Queen Elizabeth Park during the first part of the  
 289 storm. At Waipu Cove Road the GIC induced by the initial decrease in  $B_x$ , seen in Figure 3,  
 290 caused the *coupon-off* potential to rise above -0.85 V, while at Queen Elizabeth Park the  
 291 potential actually became more negative. Again, as for the *PSP-off* this is related to the  
 292 difference in phase of variations due to GIC depending on the location of the site.

293 Table 2 shows that the *coupon-off* potential also rose above -0.85 V at Komokoriki Hill  
 294 Road (KHR), Mahoenui (MOH), Lower Duthie Road (DR), Tempsky Road (TPY) and Tumunui  
 295 Block (TB), although, apart from at Lower Duthie Road, the mean level of the potential was  
 296 above or very close to this value. At Lower Duthie Road, where the sampling interval of *coupon-*  
 297 *off* potential was 60 minutes, only a single measurement in the 96 hours shown exceeded this  
 298 value. Similarly, the *coupon-off* potential became lower than -1.2 V at seven of the sites listed in  
 299 Table 2. At Waipu Cove Road (WCR), Pembroke Road (PR), Takapu Road (TakR) and Whatatutu  
 300 Road (WhR) the mean level of the potential was slightly lower than this value. The most  
 301 extreme negative potentials by far were seen at Waipu Cove Road and Queen Elizabeth Park  
 302 (QEP). At the latter site the range of variation was such that almost 30% of the *coupon-off*  
 303 potentials measured over 96 hours were outside the desired range of -0.85 to -1.2 V. The vast

304 majority of these were during the 48 hour period from 1200 UT 10 May 2024 to 1200 UT 12  
305 May 2024.

306 *Coupon-off* potentials were not measured at Raukawa Road where, as seen in Table 1  
307 and Figure 5, there were large variations in values of *PSP* when the rectifier was turned off. As  
308 might be expected, and as is discussed below, there is a close correlation between variations in  
309 such pipe to reference cell measurements and *coupon-off* measurements. That being the case it  
310 can be inferred that large variations in the cathodic protection level, as given by *coupon-off*  
311 measurements, similar in magnitude to those seen at Waipu Cove Road, are also very likely to  
312 have occurred at Raukawa Road.

| Site | 0000 UT 10 May 2024 – 0000 UT 14 May 2024 |                              |                              |                     |
|------|---|------------------------------|------------------------------|---------------------|
|      | Mean coupon-off potential (V)             | Max coupon-off potential (V) | Min coupon-off potential (V) | Sample interval (m) |
| SR   | -1.098                                    | -0.107                       | -1.315                       | 5                   |
| WCR  | -1.426                                    | 0.526                        | -2.556                       | 5                   |
| KHR  | -0.853                                    | -0.798                       | -0.916                       | 5                   |
| AR   | -1.130                                    | -0.653                       | -1.167                       | 5                   |
| MOH  | -0.794                                    | -0.742                       | -0.850                       | 60                  |
| PR   | -1.261                                    | -1.247                       | -1.271                       | 60                  |
| DR   | -1.068                                    | -0.508                       | -1.199                       | 60                  |
| TPY  | -0.763                                    | -0.731                       | -0.786                       | 60                  |
| QEP  | -0.974                                    | 1.503                        | -2.429                       | 10                  |
| TakR | -1.285                                    | -0.683                       | -1.312                       | 10                  |
| TB   | 0.026                                     | 0.127                        | -0.138                       | 10                  |
| WaR  | -1.174                                    | 0.563                        | -1.343                       | 10                  |
| WhR  | -1.294                                    | -1.259                       | -1.337                       | 10                  |

Table 2: Mean, maximum and minimum values of coupon-off potentials for the period 0000 UT 10 May 2024 to 0000 UT 14 May 2024. Values shown in red are those outside the -0.85 to -1.2 V range.

313 Although both *coupon-off* and *PSP-off* potentials can be considered as indicators of the  
314 efficacy of cathodic protection on the pipeline, the relationship between them is not simple. At  
315 most sites where the *PSP-off* potential both reached highly negative values and become  
316 positive at times, such as Salle Road, Takapu Road and Waimana Road, there are three distinct  
317 features in the relationship between *coupon-off* and *PSP-off* potentials, as shown in Figure 8. At  
318 highly negative *PSP-off* potentials the *coupon-off* potential approaches a constant value. This  
319 asymptotic behavior has been discussed by Ackland & Dylejko (2019) and related to the  
320 electrochemical equilibrium between Fe in an aqueous environment and Fe<sub>3</sub>O<sub>4</sub>. At intermediate  
321 values of *PSP-off* the relationship between the two potentials is highly linear. This linearity  
322 breaks down at higher values of *PSP-off* when the corresponding values of *coupon-off* potential

323 become very scattered, although at some sites (e.g., Waimana Road) there is an indication that  
324 there may also be a limiting upper value of *coupon-off* potential.

325 At other sites, such as Komokoriki Hill Road and Whatatutu Road, also shown in Figure  
326 8, where the variations in *PSP-off* are not as extreme, only the linear portion of this relationship  
327 is apparent and there is no obvious indication of the asymptotic approach to a lower limit of  
328 *coupon-off* potential at highly negative *PSP-off*. Apart from Komokoriki Hill Road and Whatatutu  
329 Road, all of the monitored sites where only linearity is observed, are ones where the pipeline  
330 has the more conductive coal-tar coating. It is therefore tempting to attribute this difference in  
331 behavior to the nature of the coating, especially as at Queen Elizabeth Park (Figure 8), where  
332 the coating is coal-tar, linearity in the relationship persists to positive values of the *PSP-off*  
333 potential.

### 334 **6 Anode bed to pipe potential variations during the Gannon Storm**

335 Although the variations in *PSP-off* and *coupon-off* potentials give a guide to locations  
336 where the pipeline may be at risk as a result of major geomagnetic activity, the relatively small  
337 number of sites where *PSP* is monitored means that the coverage is somewhat limited. The  
338 potential between the anode bed and the pipe (*APP*), however, is monitored at every rectifier  
339 and gives the most widespread coverage of the effect of GIC on the network. *APP* can be  
340 regarded as the sum of a potential drop (*IR*) between the anode bed and the ground  
341 immediately adjacent to the pipe, essentially the rectifier current times the ground  
342 “resistance”, and the potential drop between the ground outside the pipe and the pipe surface.  
343 This second term can effectively be regarded as the negative of the *PSP*, hence

$$344 \quad APP = IR - PSP \quad (4)$$

345 As is discussed further below, the rectifier current is constant except during major rapid  
346 changes in potential and the term *IR* may therefore, to a very good approximation, be  
347 considered as constant over the duration of a storm. This means that, if the mean value of *APP*  
348 is subtracted from *APP*, and the mean value of *PSP* is subtracted from *PSP*, the resulting  
349 potentials (*APP<sub>0</sub>* and *PSP<sub>0</sub>*) are related by

$$350 \quad APP_0 = -PSP_0 \quad (5)$$

351 The anode to pipe potential variations treated in this manner can be seen as a guide to how *PSP*  
352 varies at sites where it is not monitored. This relationship is illustrated in Figure 9 which shows,  
353 for Salle Road, both the measured *PSP<sub>0</sub>* and *-APP<sub>0</sub>*. The correlation coefficient between the  
354 two series is 0.992. Also shown are plots of *PSP<sub>0</sub>* and *-APP<sub>0</sub>* when the rectifier was turned off.  
355 The similarity between these suggests that at sites where pipe to reference cell potentials are  
356 not measured, the anode to pipe potentials when the rectifier is turned off can be used as a  
357 suitable proxy for assessing the behavior of the cathodic protection system at that site.

358 Measured anode bed to pipe potentials from four locations are shown in Figure 10. The  
359 absolute range of the variations in *APP* differs from site to site, the largest, approximately 7 V,

360 being at Waitao Road which is on the coast in the Bay of Plenty (Figure 1). At this site the *APP*  
361 actually became negative for a short period of time at just after 0730 UT on 11 May 2024. At  
362 the other three sites the range of the variations is between 1.5 and 4.5 V. Apparent from Figure  
363 10, as is the case for *PSP*, is a  $180^\circ$  phase difference between variations at Timaru Road and Te  
364 Horo Beach Road when compared to Waitao Road and Shewan Road. Also noticeable is a  
365 difference between the average *APP* at the four sites. This is significantly higher at Timaru  
366 Road and Te Horo Beach Road ( $> 10$  V) than at either Waitao Road or Shewan Road ( $< 5$  V). This  
367 difference in the average level of *APP* is related to the different pipeline coatings, and is  
368 significantly higher on those sections of pipeline (principally from Taranaki north to Auckland  
369 and south to Wellington) which are coated with coal-tar compared to those coated with more  
370 modern and less conductive coatings. It results from the necessity for a higher rectifier output  
371 voltage being required to supply the necessary current and negative potential to the pipe on  
372 coal-tar coated sections.

### 373 **7 Rectifier current “collapse”**

374 As detailed above the rectifiers supplying the cathodic protection to the New Zealand  
375 pipeline network are set to provide a constant current. Thus, except in cases of rapid magnetic  
376 field variations there is little change in current (e.g. Figure 2, Ingham et al., 2022). During the  
377 Gannon Storm, however, at some locations there were major variations in rectifier output  
378 current. These included not only significant increases in current but also some instances where  
379 the current dropped to zero. Such occurrences were at sites where major variations in the  
380 observed pipe to reference cell potential occurred. An example, from Waipu Cove Road, is  
381 shown in Figure 11.

382 This behavior can be understood by recalling that, just as the measured pipe to  
383 reference cell potential is made up of separate parts, as expressed in equation (1), the anode to  
384 pipe potential (*APP*) is made up of two parts – the potential difference supplied by the actual  
385 rectifier, and a potential due to GIC. The left hand panels of Figure 12 show an expanded time  
386 section of the variations in rectifier current output and pipe to reference cell potential at Waipu  
387 Cove Road over a period of 5 hours. Four major instances where the output current effectively  
388 became zero are marked. It is apparent that these “collapses” of current supply occurred when  
389 the pipe to reference cell potential became more negative than a limit shown by the red  
390 horizontal dashed line. It can be inferred that at these times the effect of GIC on the pipe was  
391 to make it sufficiently negative that no current was required from the rectifier itself to supply  
392 the cathodic protection – in effect protection was being supplied by the GIC. In contrast, when  
393 the pipe to reference cell potential increased, including above zero, the rectifier current was  
394 either above or at its normal constant value. Inspection of the effect on the measured coupon-  
395 off potentials suggests that it is only during these rapid increases in *PSP* that there is a  
396 significant change, with *coupon-off* potentials, as evidenced in Figure 7 also rising, sometimes  
397 above the  $-0.85$  V level. This relates to the fact that the actual output voltage of the rectifier is  
398 limited and cannot rise above a set maximum value.

399 The upper right-hand panel of Figure 12 shows the anode to pipe potential when the  
400 rectifier was turned off. This is essentially the contribution to the anode to pipe potential  
401 resulting from GIC. The instances of current collapse coincide with increases in *APP-off* above a  
402 certain level, again indicating that GIC are causing the pipe to be sufficiently negative that it is  
403 protected. If the *APP-off* potential represents the contribution of GIC to measured *APP*, then  
404 subtracting this from the measured *APP* immediately before rectifier turn-off gives an  
405 approximation to the actual output voltage of the rectifier. This is shown in the lower right-  
406 hand panel of Figure 12, and shows, within the limits of the 5-minute sampling at Waipu Cove  
407 Road, that the rectifier output voltage does indeed decline dramatically during the periods of  
408 current collapse.

## 409 **8 Towards predicting extreme storm pipeline effects**

410 It is apparent from the results presented above that during the Gannon Storm  
411 measurements of both *PSP-off* and *coupon-off* potential indicate that certain sites on the New  
412 Zealand pipeline network showed variations in these quantities which took the pipe outside the  
413 desired cathodic protection range. The estimated corrosion rate at these sites, due to rises in  
414 *PSP*, caused by this single *Kp* max 9- to 9 storm was about 0.15 mm/year. Despite the added  
415 knowledge gained from the Gannon Storm, the likelihood of disbonding due to large decreases  
416 in *PSP* still remains unquantified, although sites subject to risk due to rises in *PSP* are, largely,  
417 also those susceptible to significant decreases in *PSP*. An “extreme” storm is estimated to have  
418 magnetic field variations at least of the order of 10 times larger than the Gannon Storm for New  
419 Zealand latitudes (Hapgood et al., 2021; Mac Manus et al., 2022), which would lead to much  
420 larger variations in both *PSP-off* and *coupon-off* potentials and, presumably, increase the  
421 estimated rate of corrosion by a similar factor. Calculating the predicted possible effects of an  
422 extreme storm on the pipeline network is therefore of significant interest. There are two  
423 potential ways in which this may be done.

424 The first method, which would allow calculation of the likely effects everywhere on the  
425 pipeline network, is through numerical modeling using the methods of Boteler and Cookson  
426 (1986) or Boteler (2013) to calculate *PSP* resulting from synthetic extreme storms. As has been  
427 discussed above, the calculated variations in *PSP* can be related to the possibility of both  
428 corrosion (including numerical calculation as per Gummow (2002)) and disbondment. At sites  
429 where a relationships between *PSP* and *coupon* potentials can be formulated such calculations  
430 may also yield the likely variations in *coupon-off* potential.

431 A second potential approach is to use measured data from the monitoring sites on the  
432 New Zealand pipeline network in a manner akin to the following.

- 433 i. At each monitoring site where data are available, use measured *PSP-on* data during  
434 multiple past geomagnetic storms to calculate transfer functions between *PSP-on* and  
435 the magnetic field variations at Eyrewell geomagnetic observatory. This is effectively  
436 similar to the approach taken by Ingham et al. (2017) to estimate GIC in the New  
437 Zealand power network. Note that the use of transfer functions between observations

438 and Eyrewell observations means that differences between the magnetic field at  
439 Eyrewell and across the North Island do not matter.

440 ii. For a synthetic extreme storm use the transfer functions to calculate the response of  
441 *PSP-on* to the storm. The type of relationship shown in Figure 5 between *PSP-off* and  
442 *PSP-on* can be used to transform this into the predicted response of *PSP-off*.

443 iii. As for the direct modelling method, observed relationships between *PSP* and coupon  
444 potentials may then, in principle, be used to calculate how *coupon-off* potentials vary.

445 iv. For locations where *PSP* are not measured a similar procedure can be used by  
446 calculating transfer functions between *APP* and the magnetic field. Relating *APP* when  
447 the rectifier is on to *APP-off*, and equation (3) can then be used to calculate the  
448 expected variations in *PSP-off*.

449 Ultimately, comparison of the results of these two approaches should give confidence in the  
450 predicted response of the network to an extreme storm. This should allow our industry  
451 partners to determine the hazard levels to their network infrastructure.

## 452 **9 Summary**

453 We have presented here observations and discussion of the effects of the Gannon  
454 Storm on the New Zealand pipeline network. The main observed features are as follows.

- 455 • Major variations in *APP*, *PSP*, and *coupon-off* potential occurred at several sites, taking  
456 the cathodic protection system outside its designated “safe” region. The sites most  
457 affected on the northern section of pipe from Auckland to Whangarei were Salle Road,  
458 Waipu Cove Road and Amriens Road. At the southern end of the pipeline network the  
459 largest variations were at Queen Elizabeth Park and Takapu Road, just to the north of  
460 Wellington. Very large variations were also seen at Raukawa Road in Hawkes Bay, and at  
461 Waimana Road in eastern Bay of Plenty. Possible corrosion rates due to the storm  
462 approached 0.15 mm/year. At several sites the average level of *coupon-off* potential  
463 was actually outside the -0.85 to -1.2 V limits, while highly anomalous potentials were  
464 observed at Tumunui Block.
- 465
- 466 • At many sites the relationship between *PSP-off* and *coupon-off* potentials shows that  
467 the *coupon-off* potential approaches an asymptotic limit at very negative values of *PSP-*  
468 *off*, but becomes scattered at high, positive, values of *PSP-off*. At other sites the  
469 relationship between these quantities is essentially linear. There is a suggestion this  
470 difference in the relationships, as well as that between mean levels of anode bed to pipe  
471 potential, may be related to the nature of the pipeline coating.
- 472
- 473 • At some sites where variations in *PSP* are large it is apparent that highly negative values  
474 of *PSP* resulting from GIC do themselves provide cathodic protection and the rectifier

475 current output and voltage drop to close to zero. There is no apparent effect on *coupon-*  
476 *off* potentials.

- 477
- 478 • At rectifier sites where pipe to reference cell potentials are not monitored the  
479 measurements of *APP* reduced to zero mean are shown to be very nearly equal to the  
480 negative of *PSP* measurements, also reduced to zero mean.

481 Study of these effects of the Gannon Storm is aiding the development of methods and  
482 procedures for predicting the possible effects of an extreme storm on the New Zealand gas  
483 pipeline network. Future studies are planned to apply those methods and hence determine the  
484 importance of space weather extreme events to this important industry.

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#### 488 **Data Availability Statement**

489 Cathodic protection monitoring data reported here are the property of First Gas New Zealand  
490 Ltd. Request for access to the data should be addressed in the first instance to Mark Sigley  
491 (mark.sigley@firstgas.co.nz). Magnetic observatory data from Eyrewell may be downloaded  
492 from [www.intermagnet.org](http://www.intermagnet.org).

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- 572
- 573

574 **Figure captions**

575 **Figure 1:** The New Zealand gas pipeline network. Red lines—pipelines coated with coal-tar  
 576 enamel; blue lines—pipelines with other, lower conductance, coatings; gray dots – earthing  
 577 beds; red dots—rectifier locations, with those used in this study named: SR – Salle Road, WCR –  
 578 Waipu Cove Road, KHR – Komokoriki Hill Road, AR – Amriens Road, ONH – Onehunga, AmP –  
 579 Ambury Park, IR - Ingram Road, TUA – Tuakau, ROT - Rotowaro Road, SWR - Shewan Road, LBR -  
 580 Lees Block Road, MOH – Mahoenui, TGP – Tongapurutu, TR - Timaru Road, PR - Pembroke  
 581 Road, DR - Lower Duthie Road, TPY - Tempsky Road, TBR - Turakina Beach Road, PPR -  
 582 Pukepuke Road, HBR - Hokio Beach Road, THBR -Te Horo Beach Road, QEP - Queen Elizabeth  
 583 Park , GR - Grays Road, TakR - Takapu Road, WTO - Waitao Road, WHE - Whites Road, JHR -  
 584 Jack Henry Road, TB - Tumunui Block, OR - Okaro Road, WaR - Waimana Road, WhR -Whatatutu  
 585 Road, WtR - Watershed Road, RR - Raukawa Road.

586

587 **Figure 2:** Schematic diagram of a CP monitoring site. Monitored quantities are: (i) the potential  
 588 between the anode bed and the pipe (*APP*), (ii) the current supplied by the rectifier, (iii) the  
 589 potential between the pipe and the Cu/CuSO<sub>4</sub> reference electrode (*PSP*), (iv) the potential  
 590 between the metal coupon and the reference electrode (*coupon*).

591 **Figure 3:** Left-hand panels show the variations in the northward ( $B_x$ ) and eastward ( $B_y$ )  
 592 components of the magnetic field recorded at Eyrewell geomagnetic observatory from 0000 UT  
 593 10 May 2024 until 0000 UT 13 May 2024. Shown in the right-hand panels are the rates of  
 594 change of  $B_x$  and  $B_y$  in nT/min.

595 **Figure 4:** Measured pipe to reference cell potential at Salle Road during the period 0000 UT 10  
 596 May 2024 to 0000 UT 13 May 2024.

597 **Figure 5:** *PSP* at Salle Road when the rectifier is turned off (*PSP-off*) plotted against the  
 598 potential immediately before turn-off (*PSP-on*). The red line shows the quadratic fit indicated.

599 **Figure 6:** Pipe to soil potentials with the rectifier turned off (*PSP-off*) calculated for 8 sites on  
 600 the pipeline network during the period 1200 UT 10 May 2024 to 1200 UT 12 May 2024. The  
 601 dashed lines mark 0 V and -2 V as discussed in the text.

602 **Figure 7:** Coupon-off potentials measured at 8 sites on the pipeline network during the period  
 603 1200 UT 10 May 2024 to 1200 UT 12 May 2024. Also shown by the dashed lines are the  
 604 recommended -0.85 V and -1.2 V limits for safe cathodic protection.

605 **Figure 8:** Coupon-off potential plotted against *PSP-off* at 6 sites. The nature of the pipeline  
 606 coating at each site is indicated: S – synthetic, CT – coal tar.

607 **Figure 9:** Measured values of the pipe to soil potential ( $PSP_0$ ) and the negative of the anode bed  
 608 to pipe potential ( $APP_0$ ), both reduced to zero mean, at Salle Road for the period 0000 UT 10  
 609 May 2024 to 0000 UT 14 May 2024. The left-hand column shows measurements when the

610 rectifier was turned on. The right-hand column shows measurements when the rectifier was  
611 turned off.

612 **Figure 10:** Anode bed to pipe potential measured at 4 sites for the 48 hours from 1200 UT 10  
613 May 2024 to 1200 UT 12 May 2024.

614 **Figure 11:** Variations in rectifier output current at Waipu Cove Road.

615 **Figure 12:** Variations in rectifier output current, pipe to reference cell potential, *APP-off*  
616 potential and calculated rectifier output over a 5 hour period at Waipu Cove Road.

617

Figure 1.

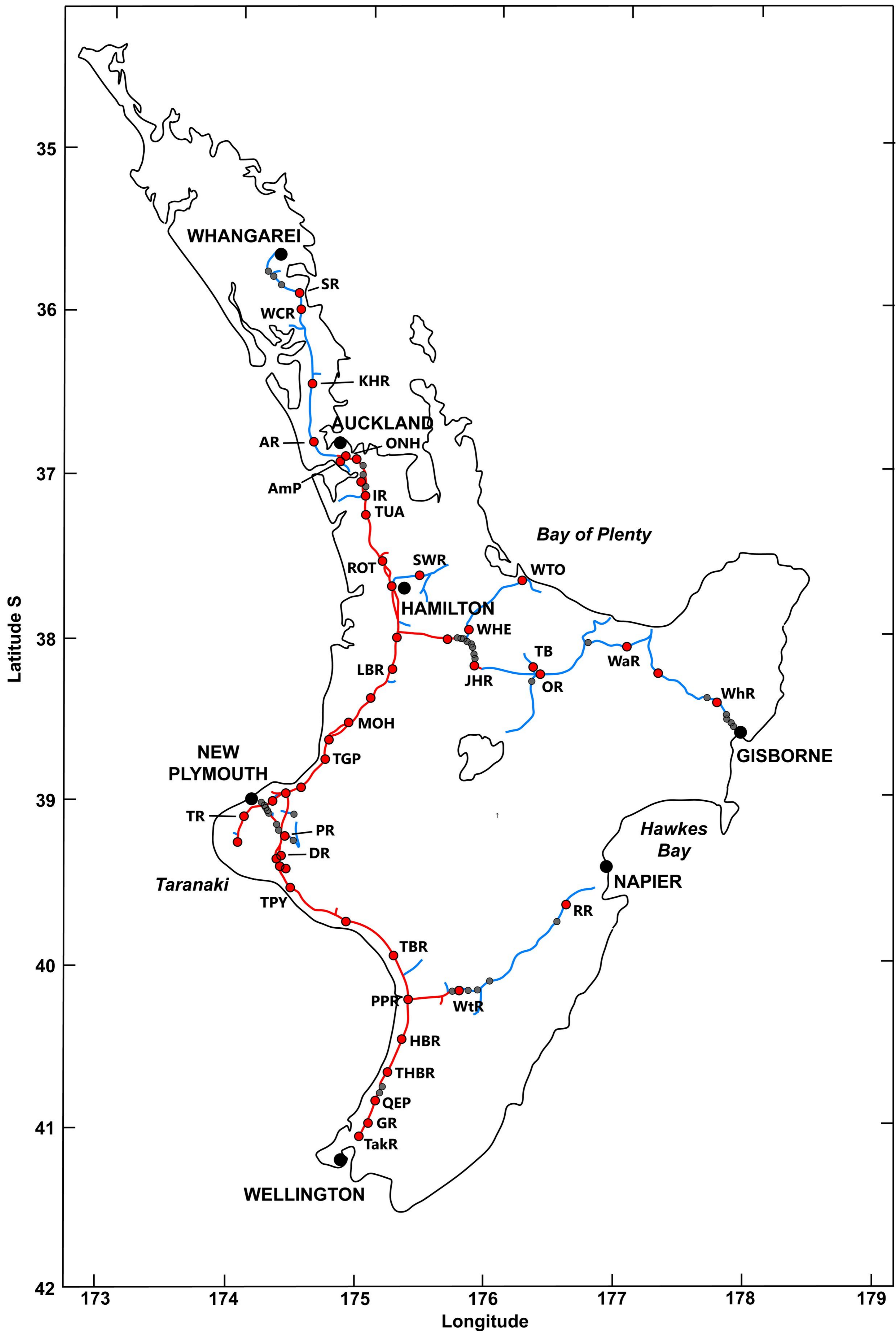


Figure 2.

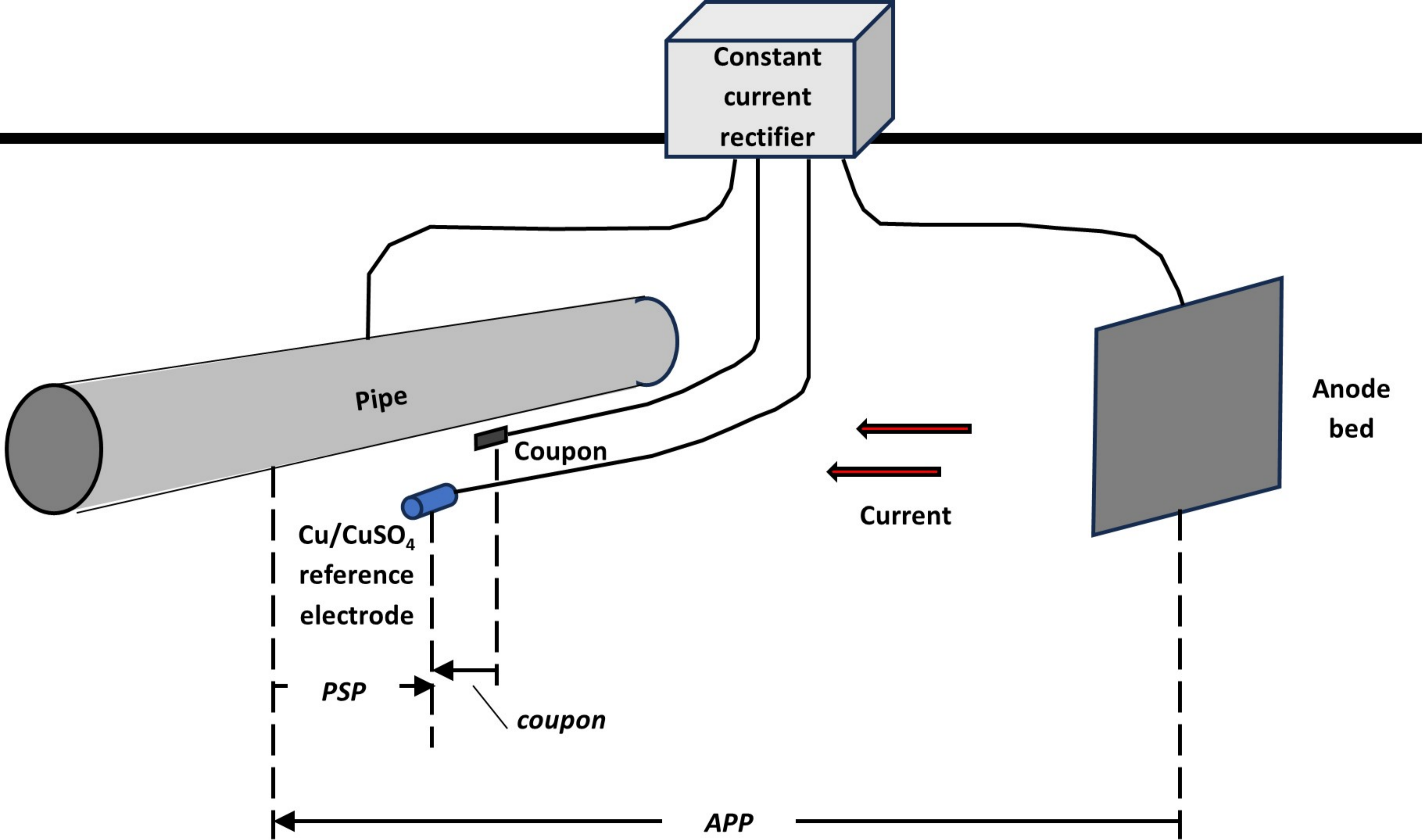


Figure 3.



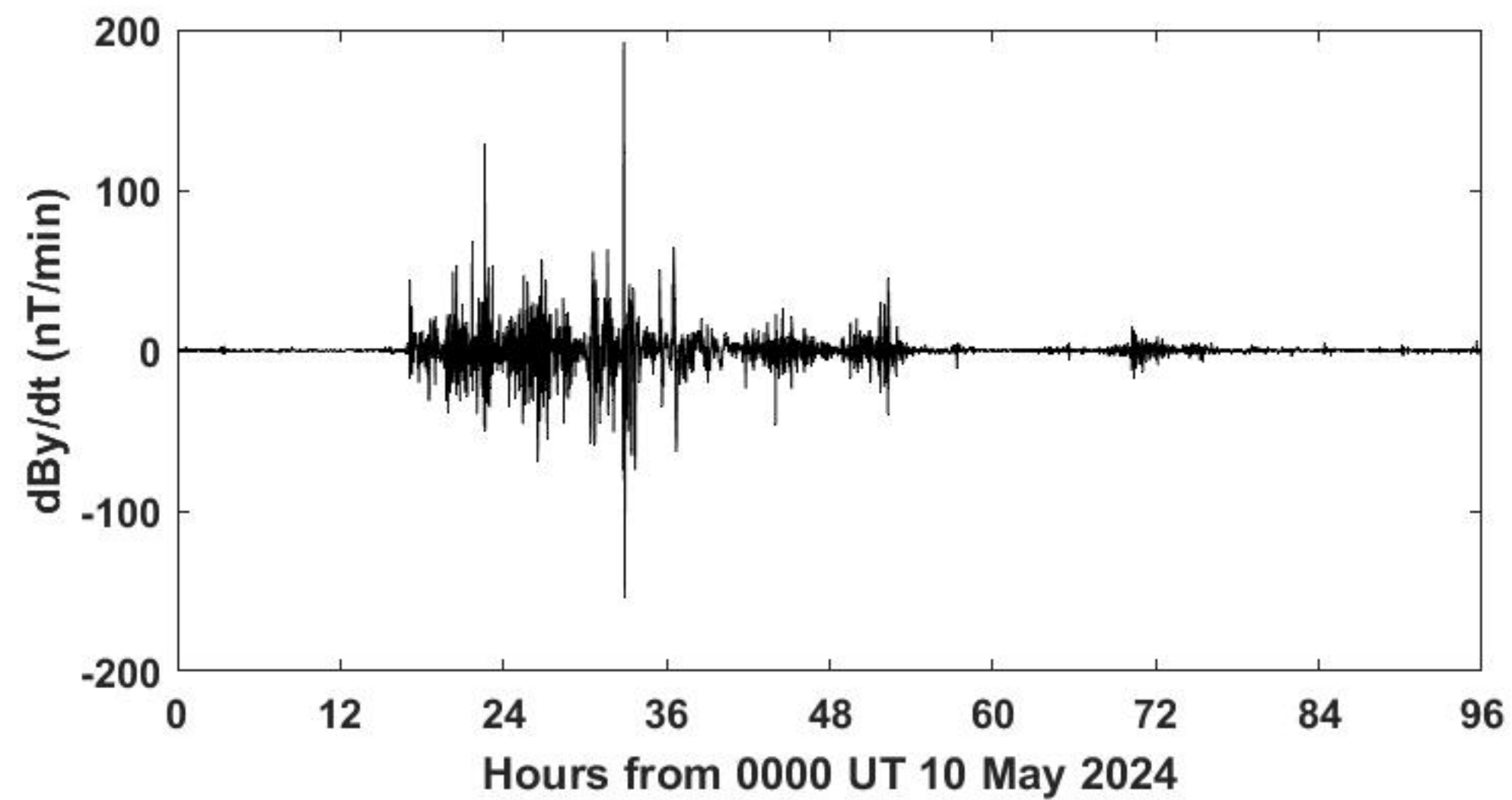
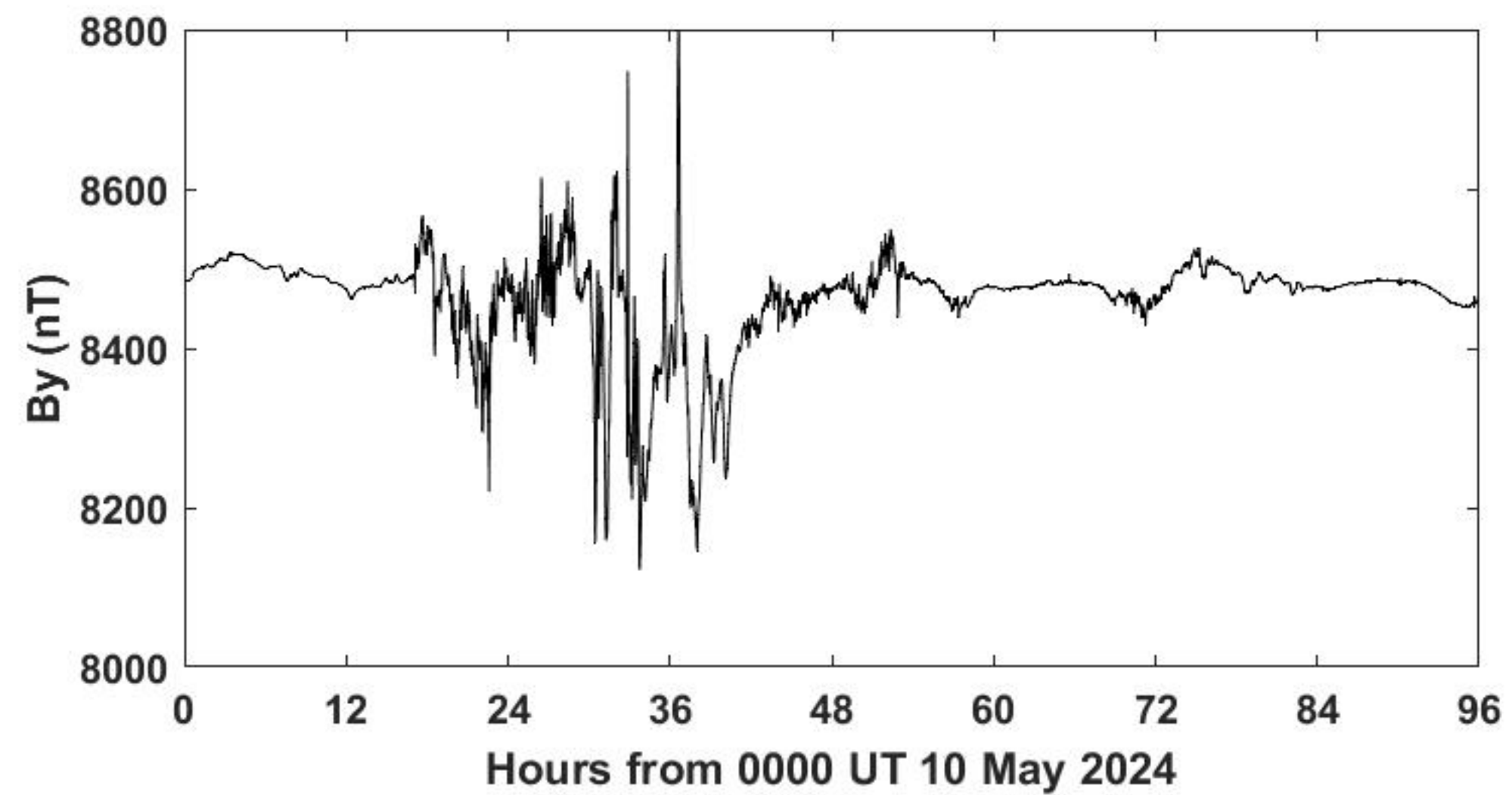
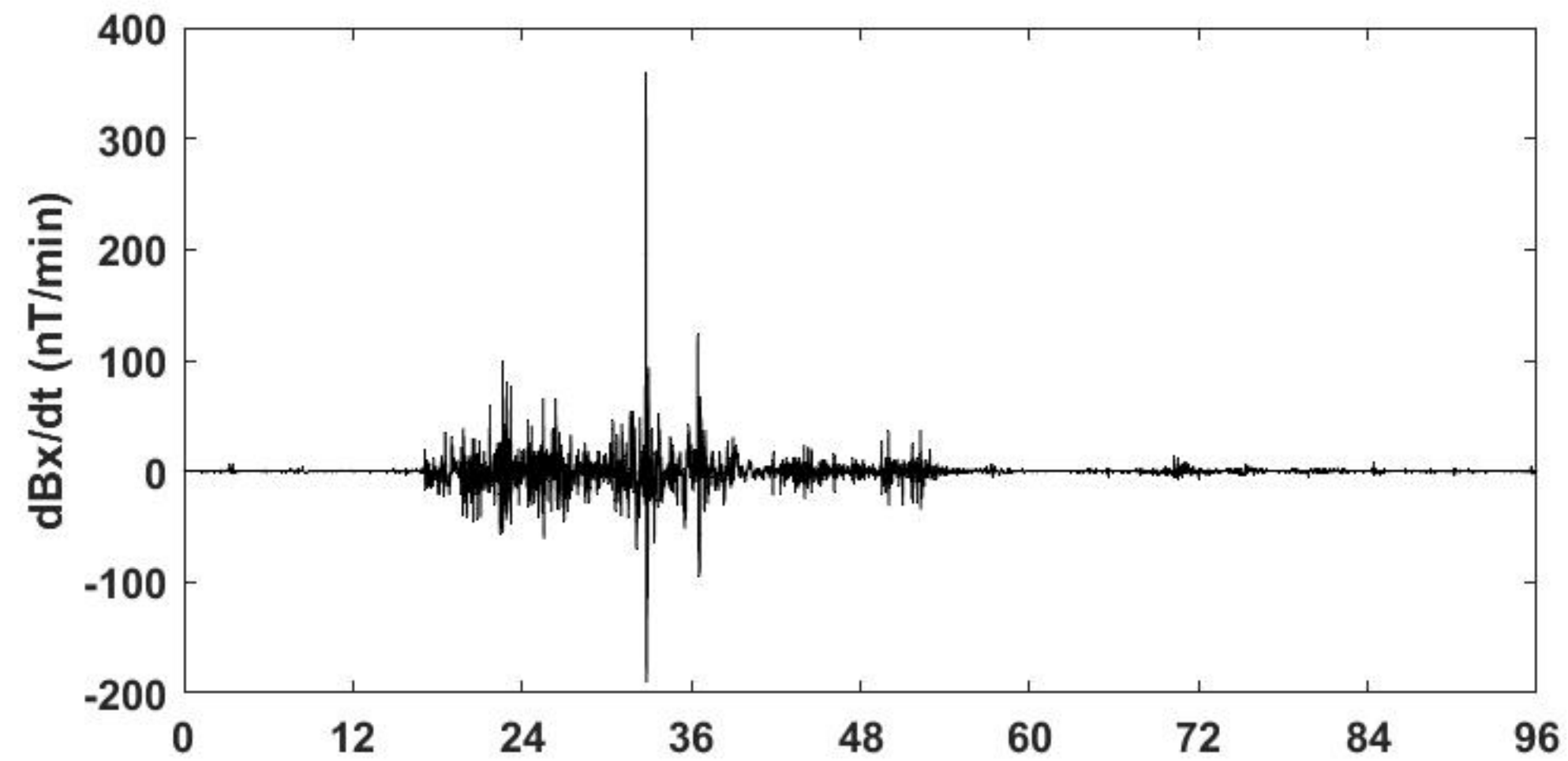
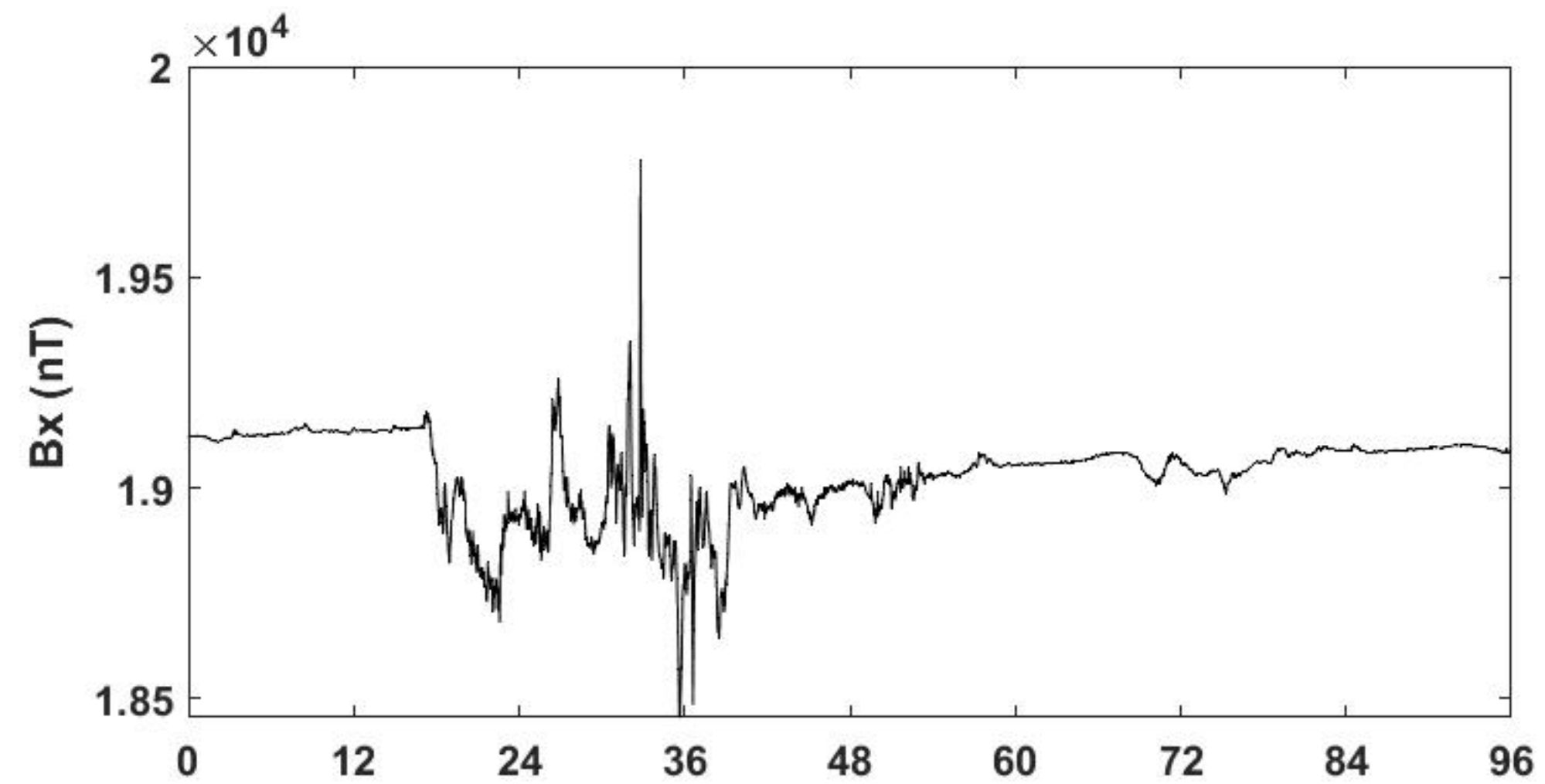


Figure 4.

# Salle Road

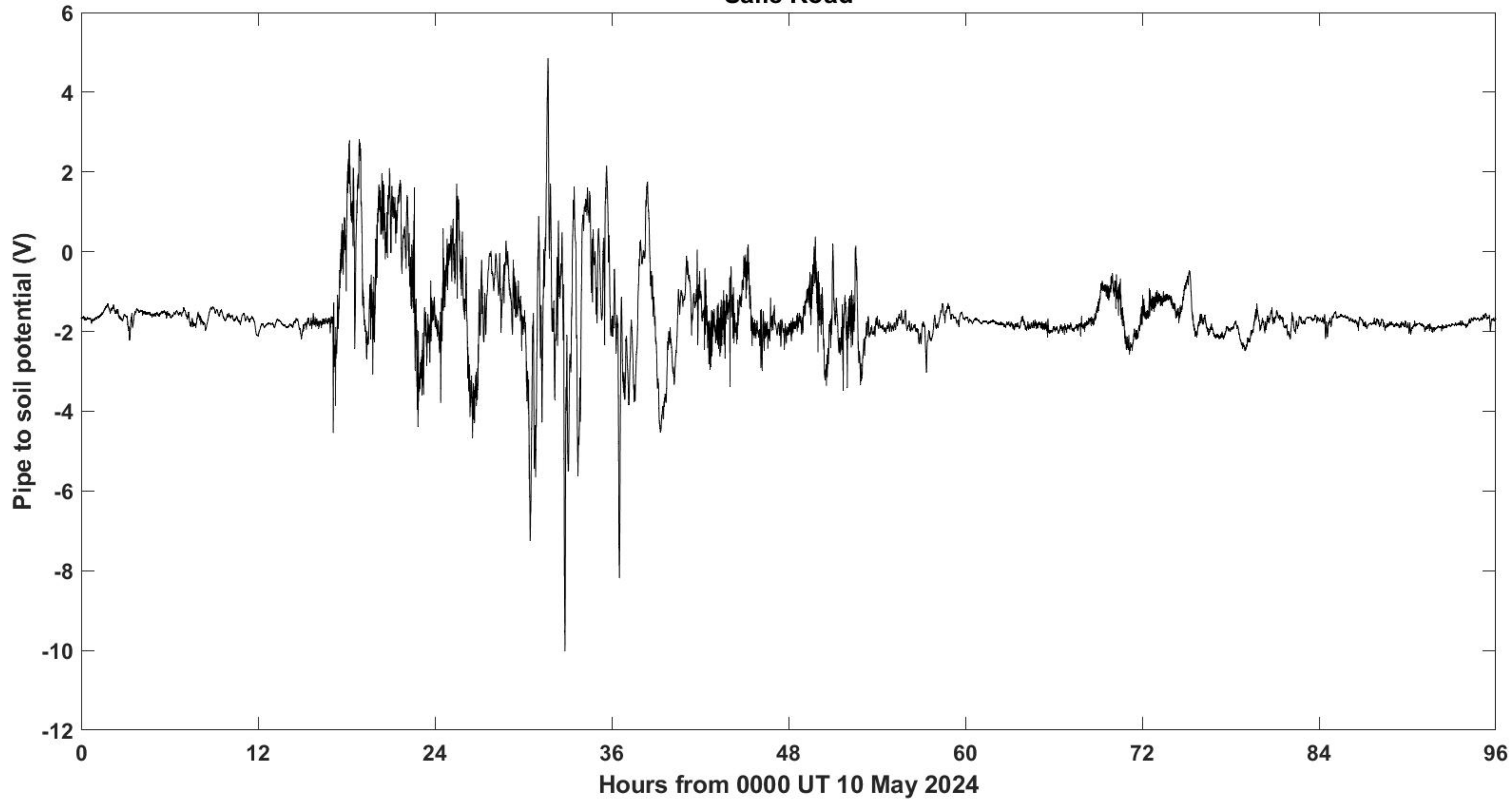


Figure 5.

# Salle Road

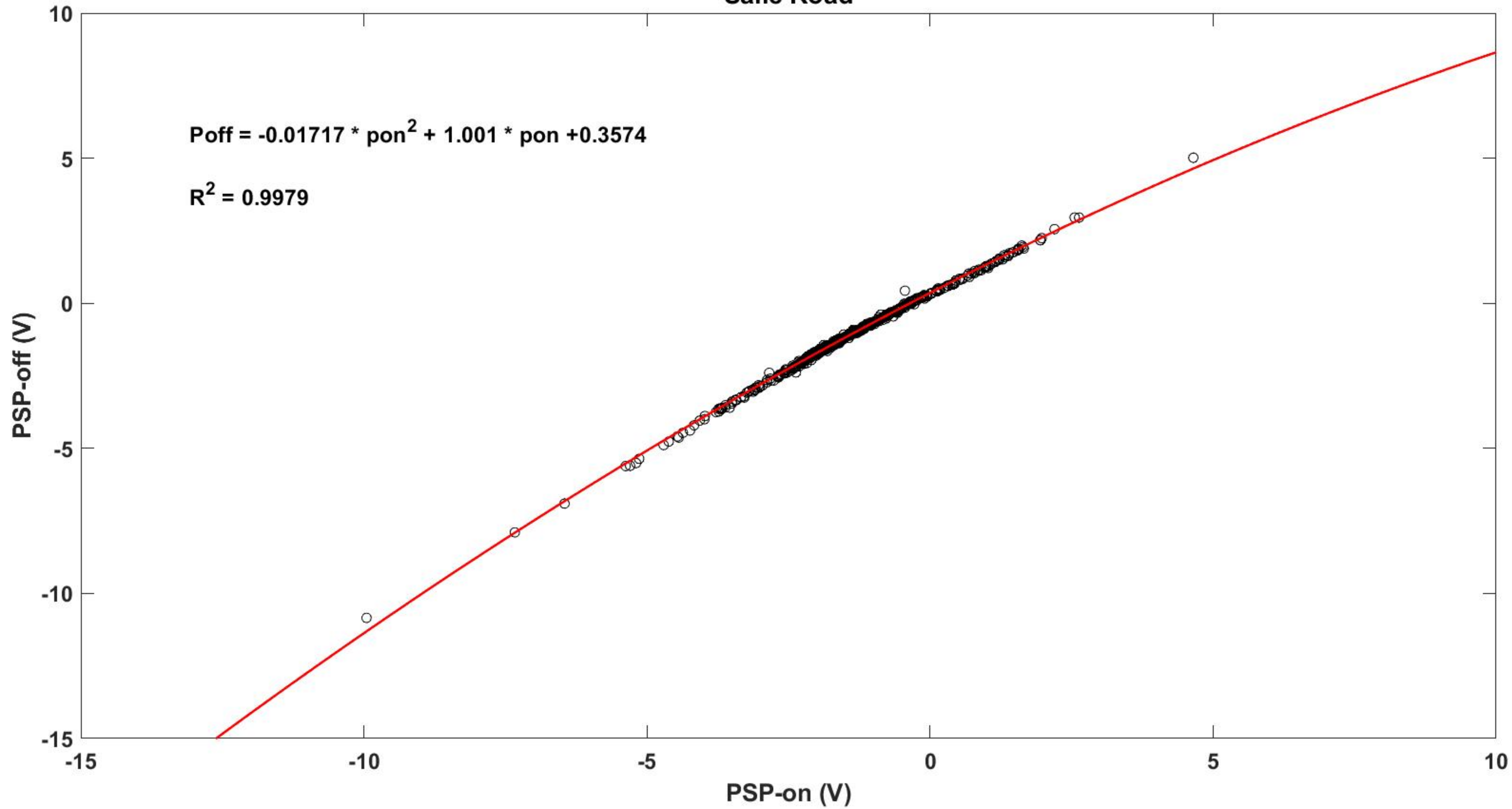
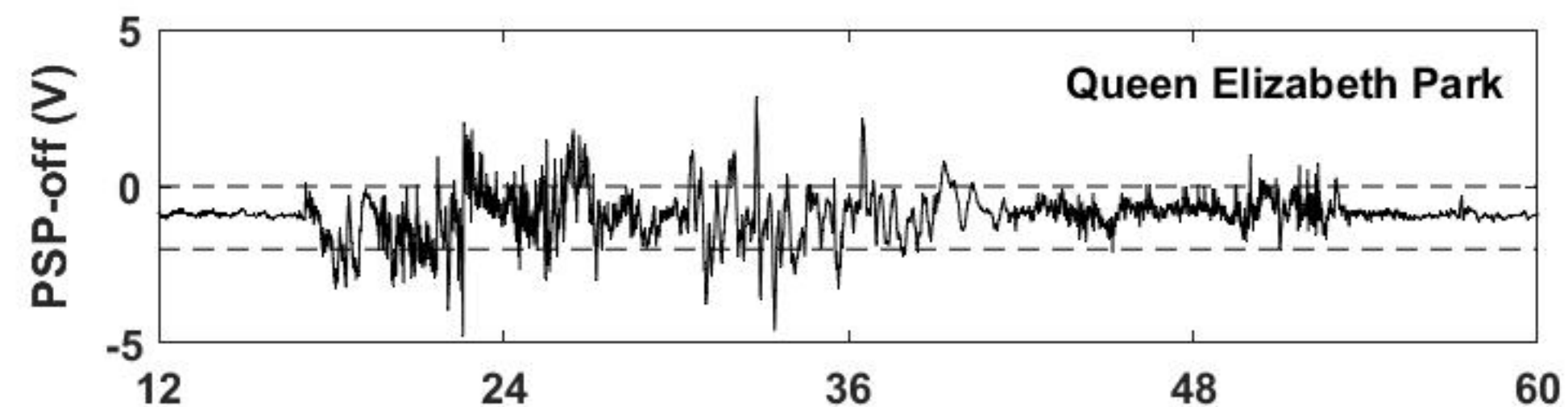
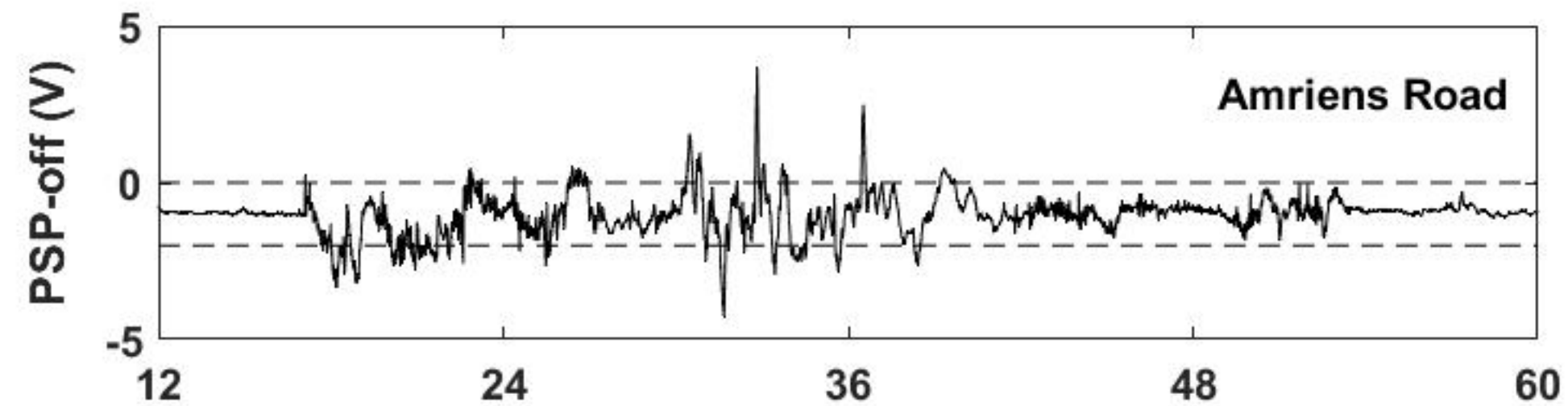
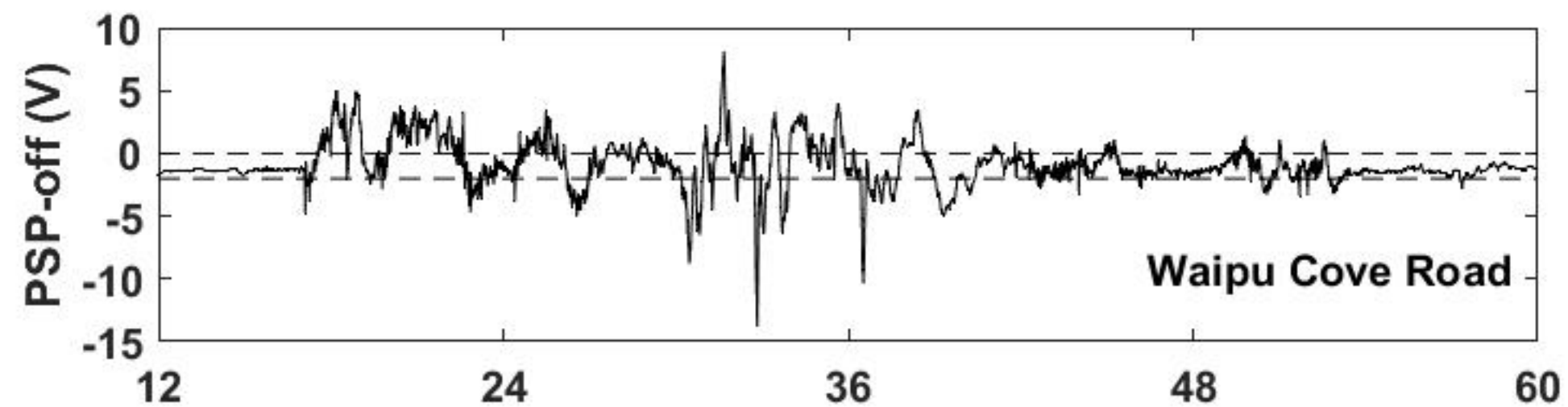
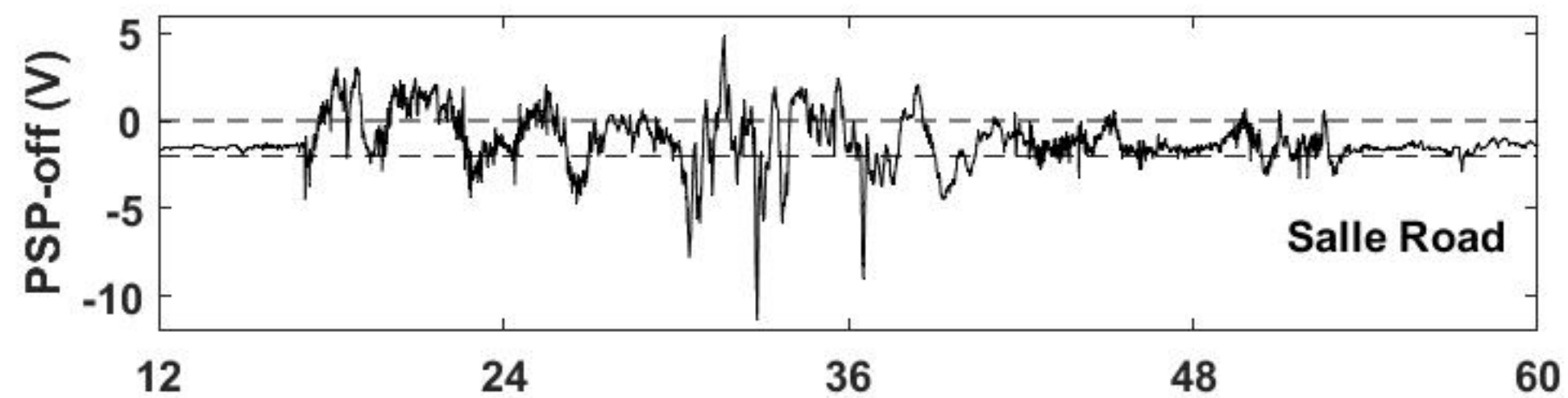
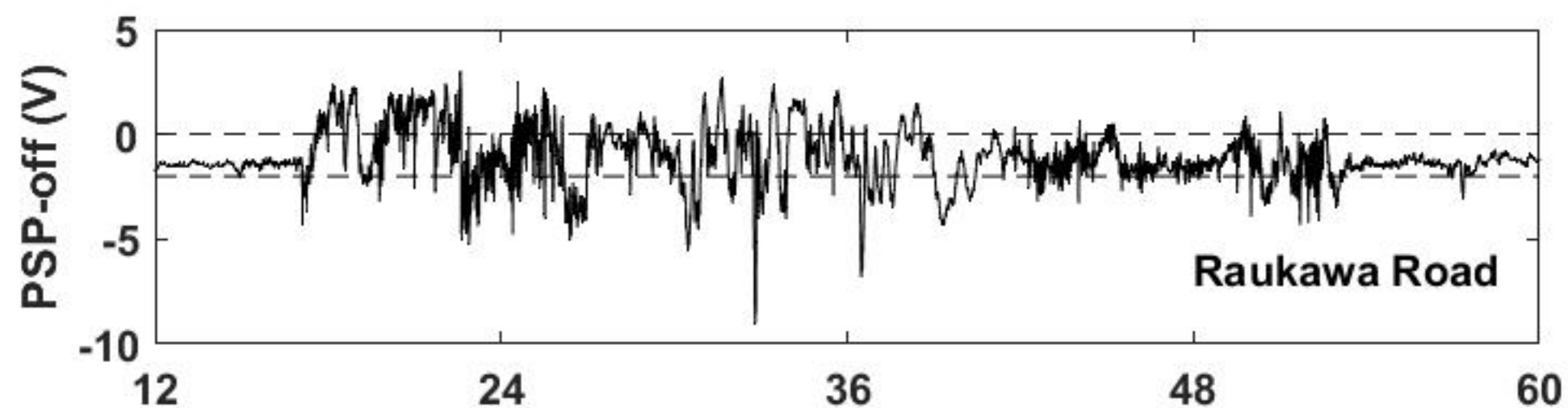
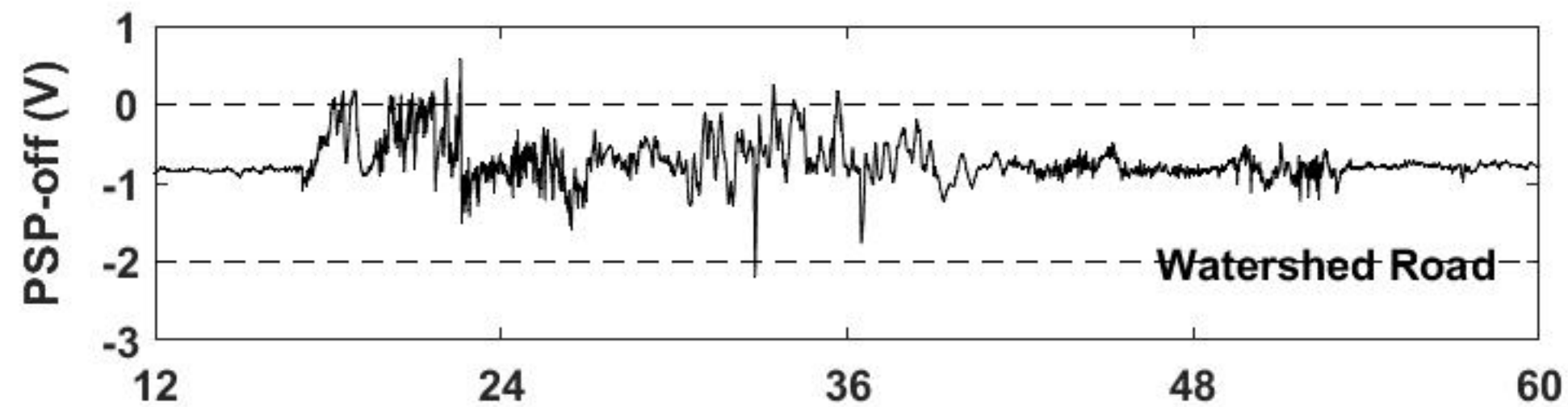
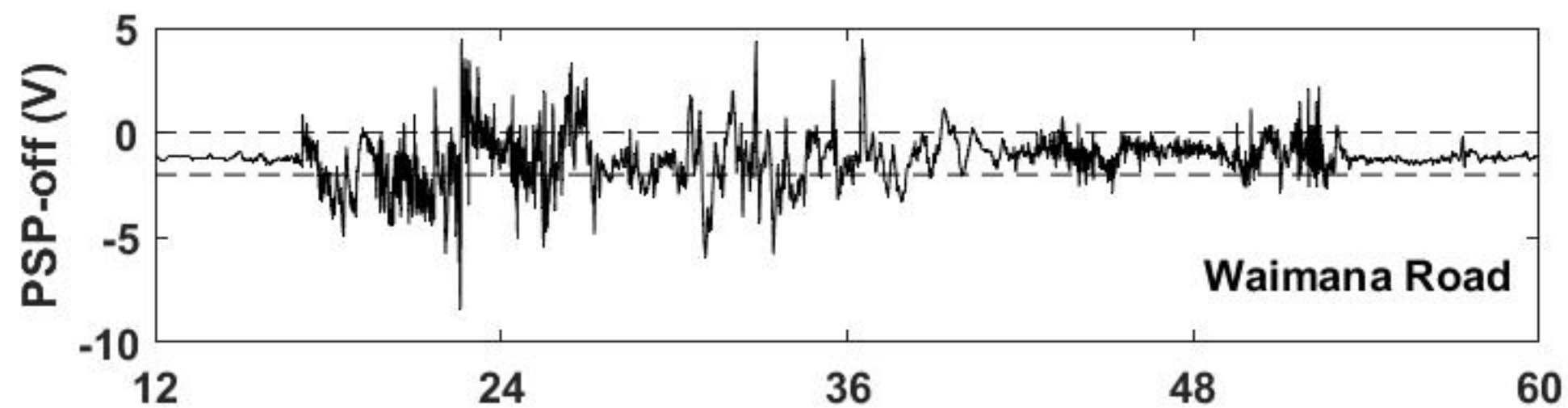
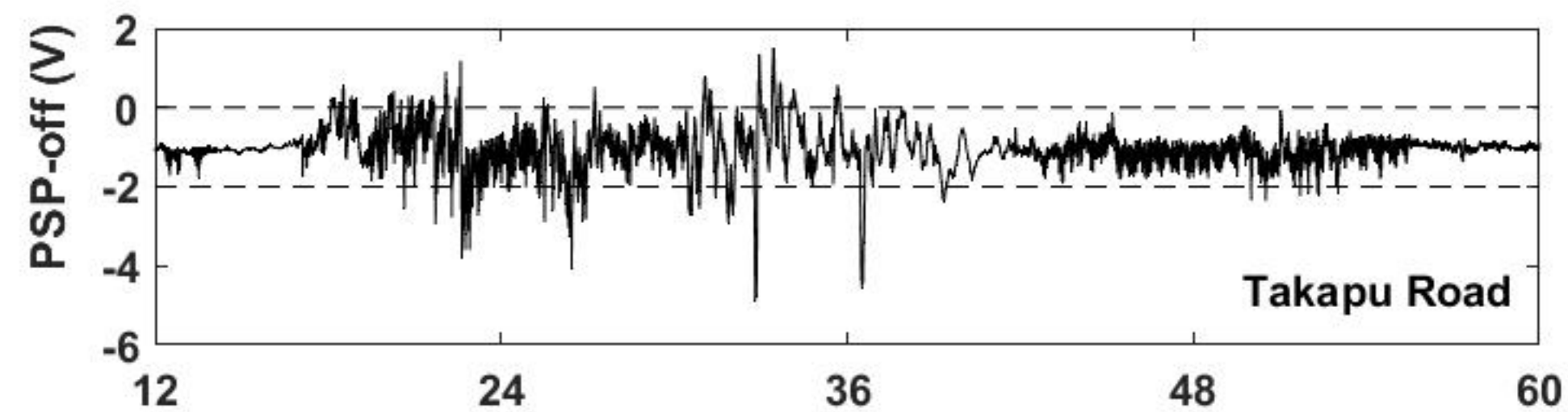


Figure 6.



Hours from 0000 UT 10 May 2024



Hours from 0000 UT 10 May 2024

Figure 7.



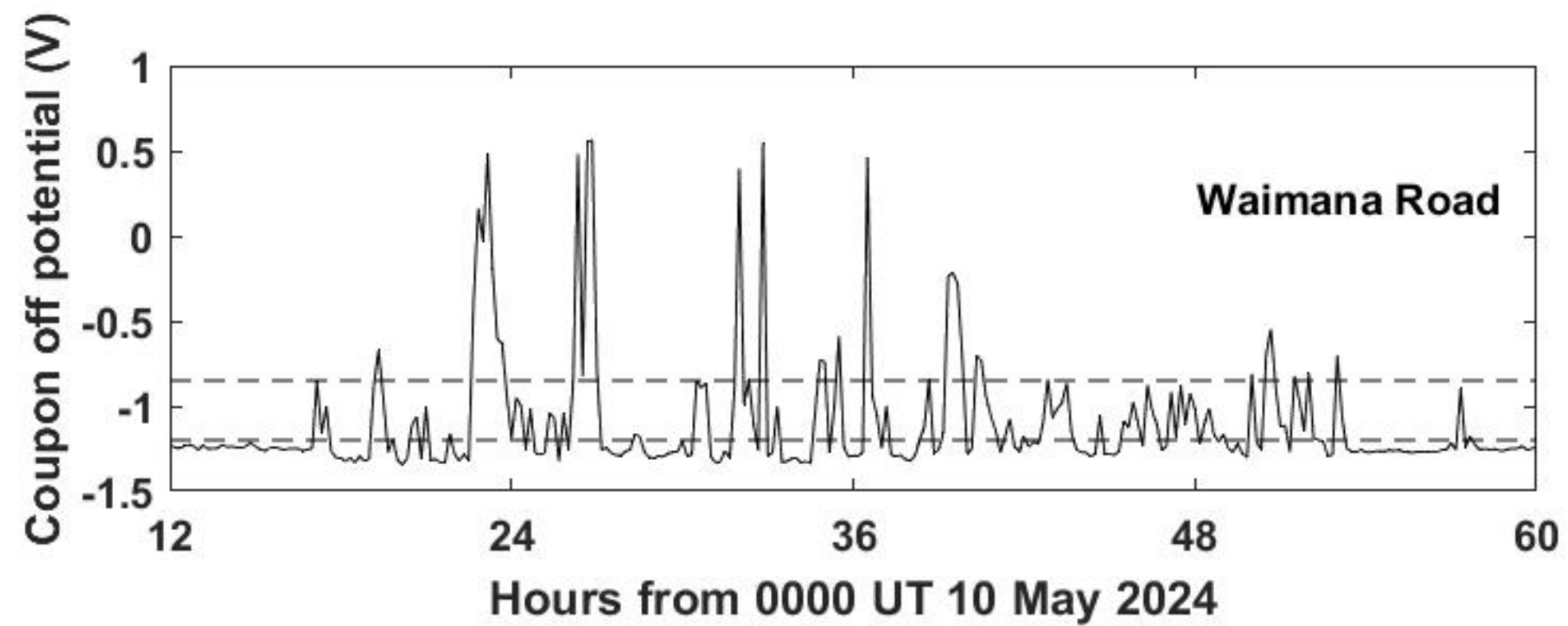
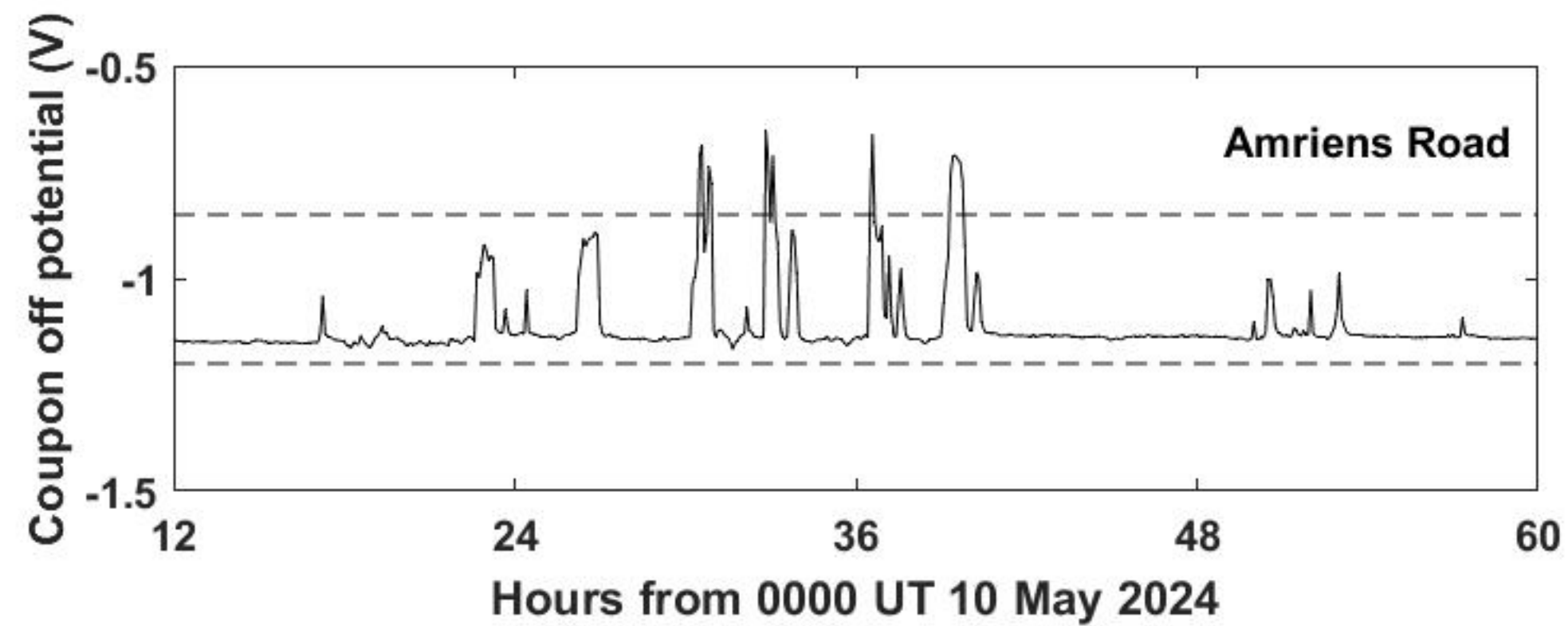
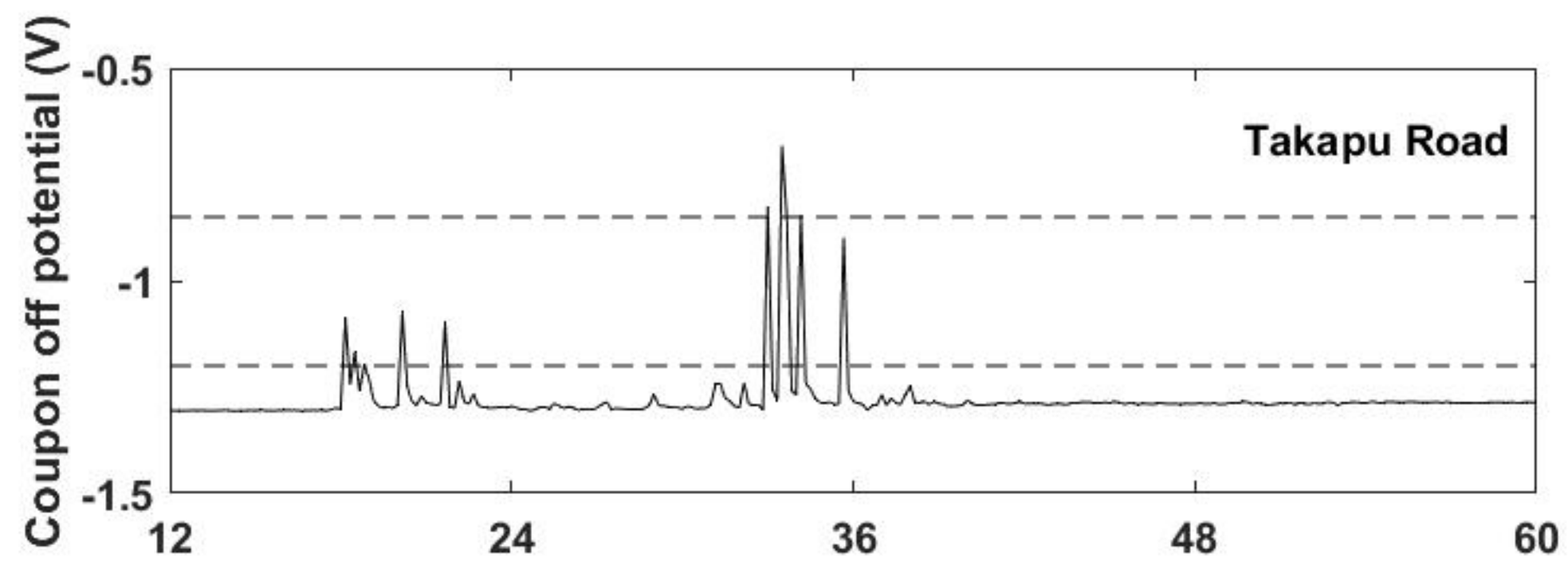
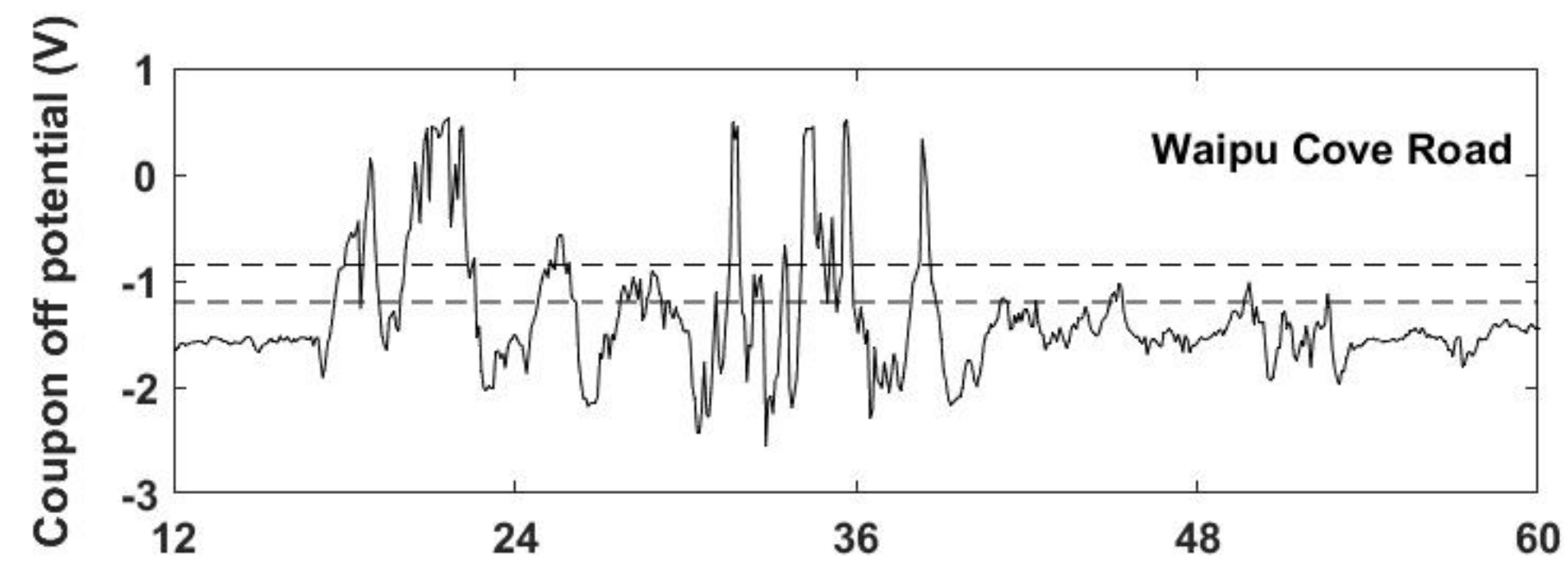
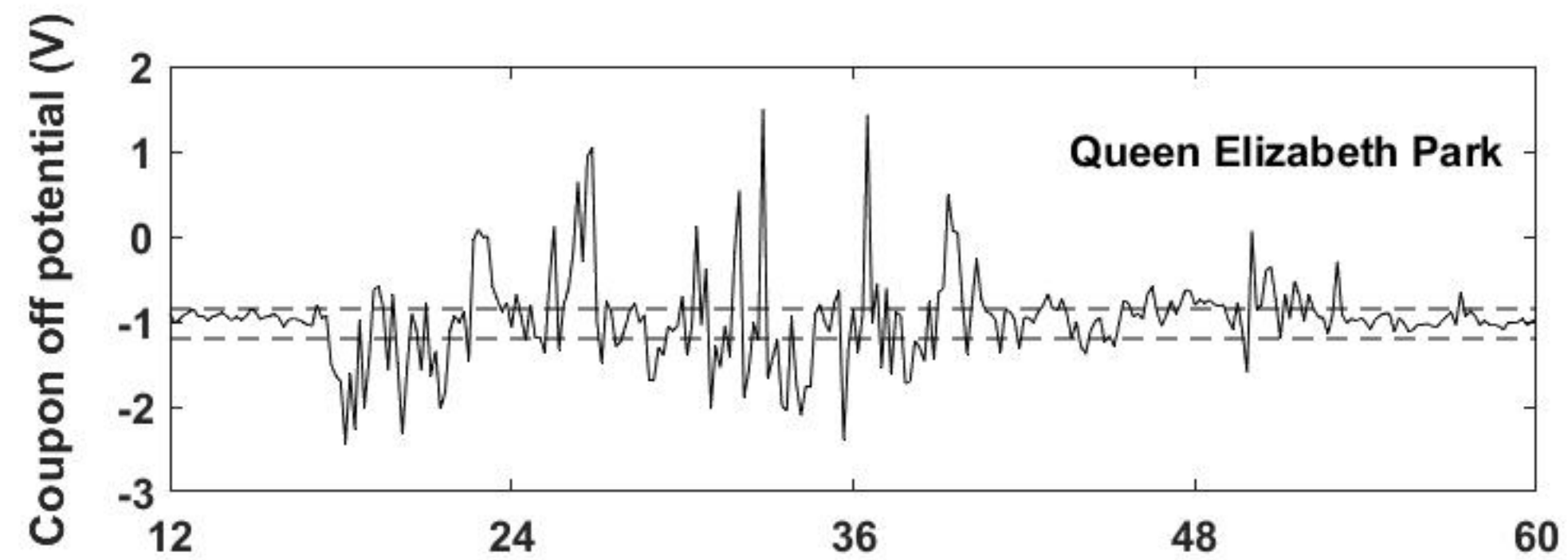
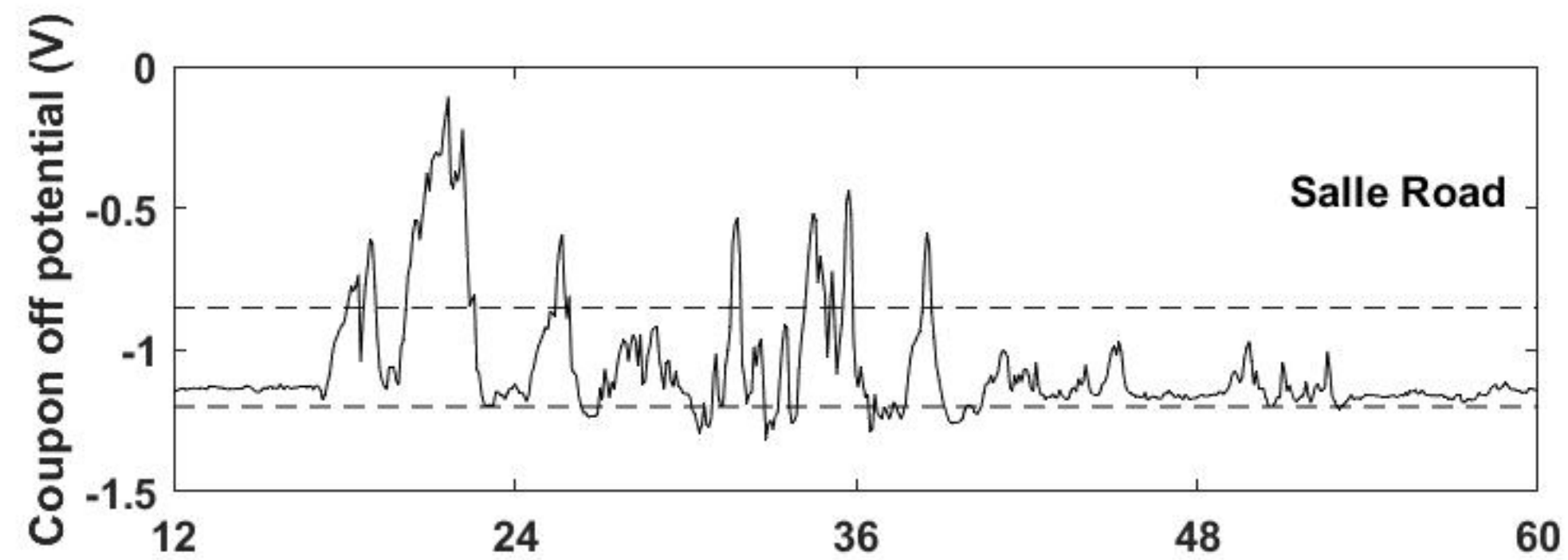


Figure 8.

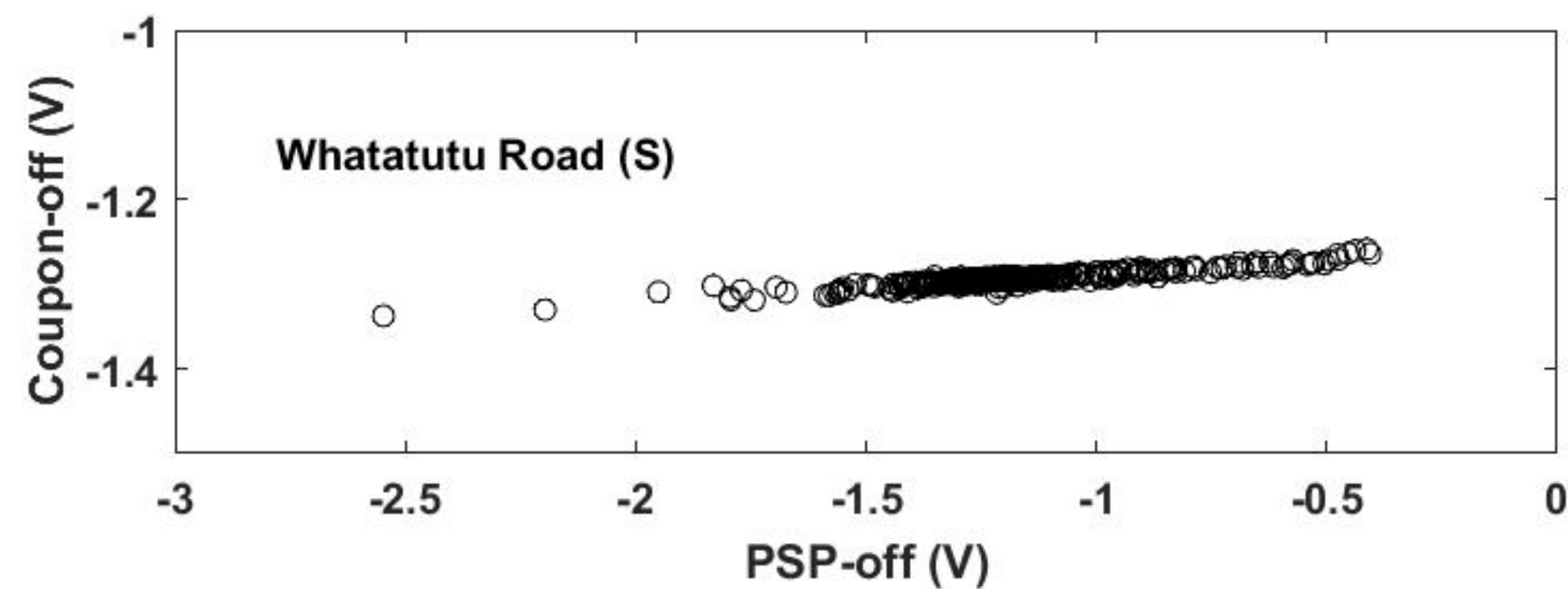
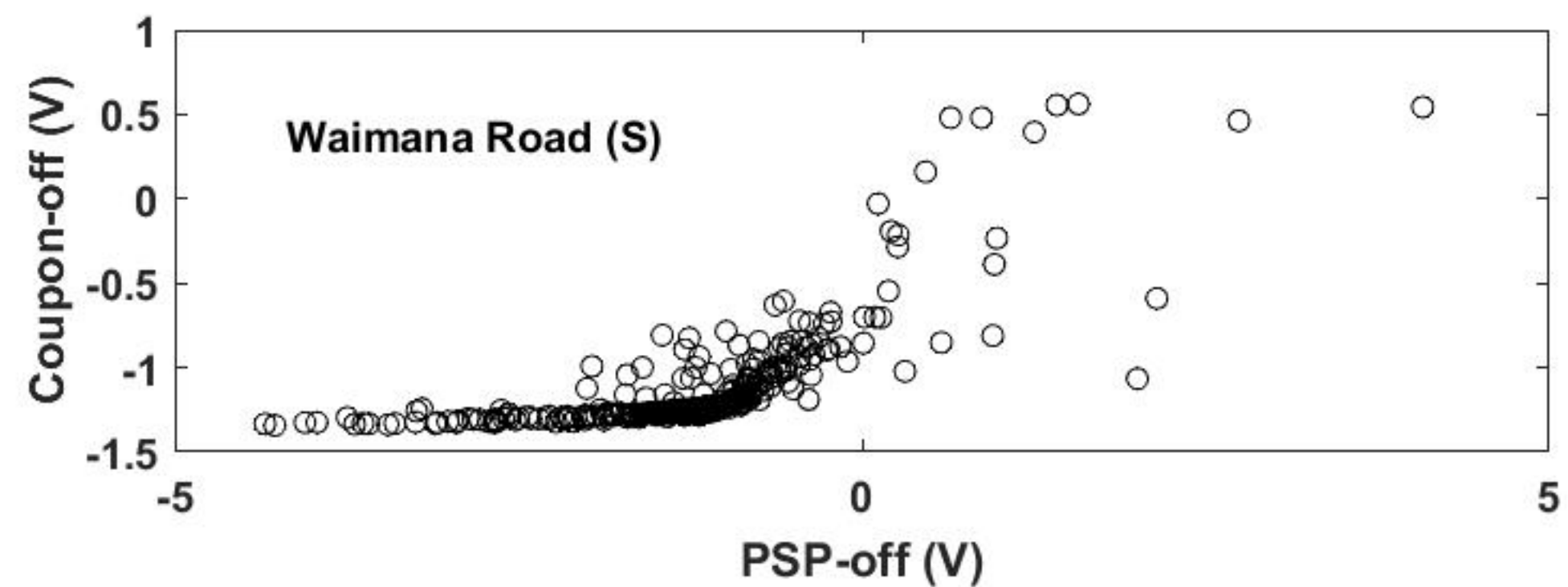
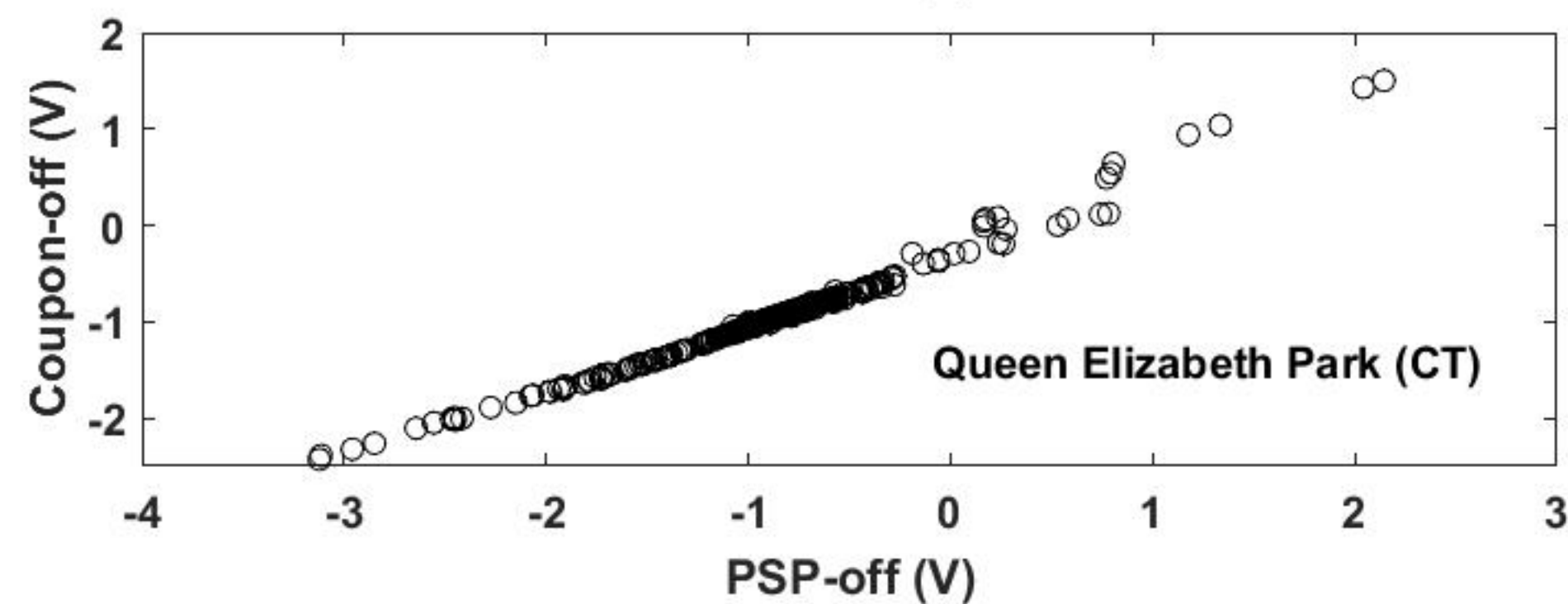
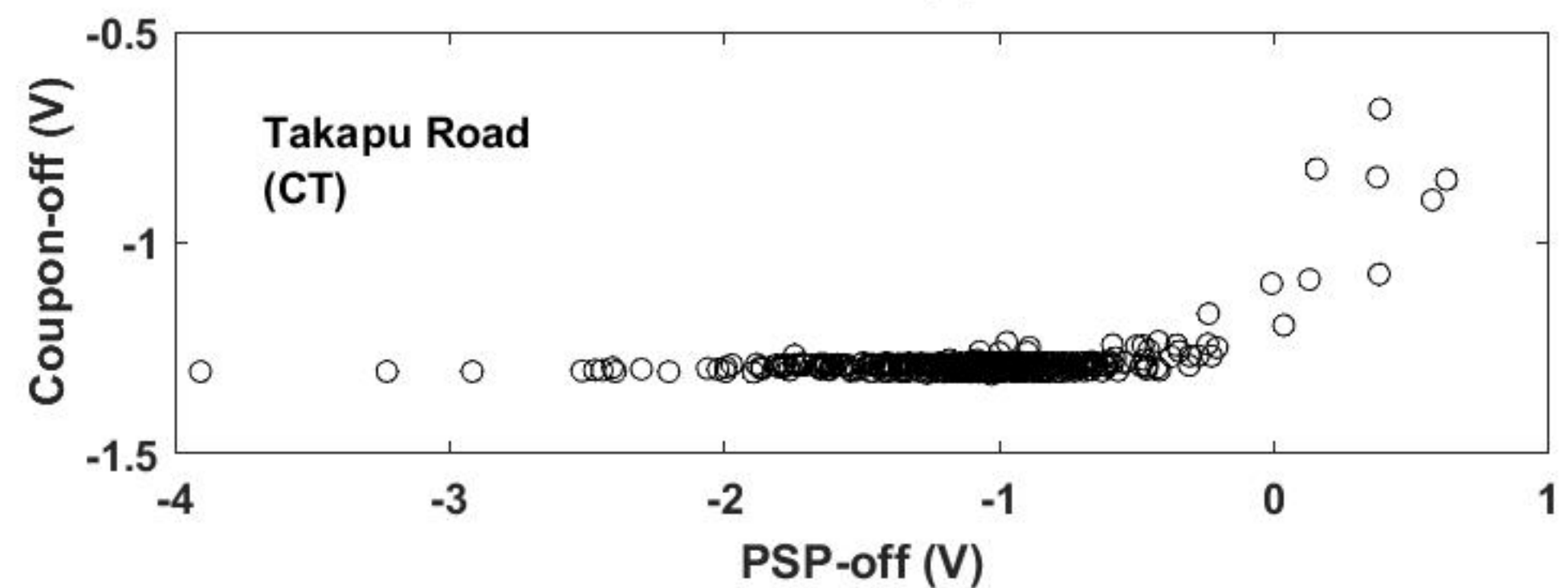
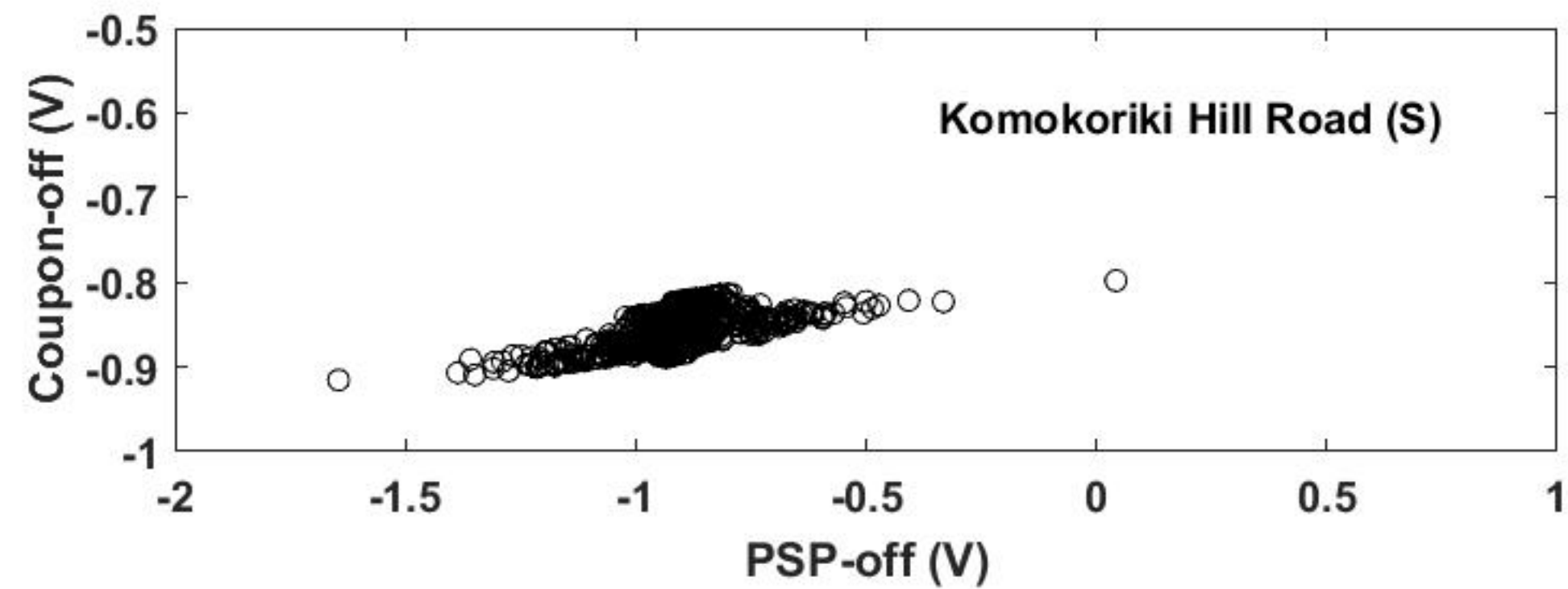
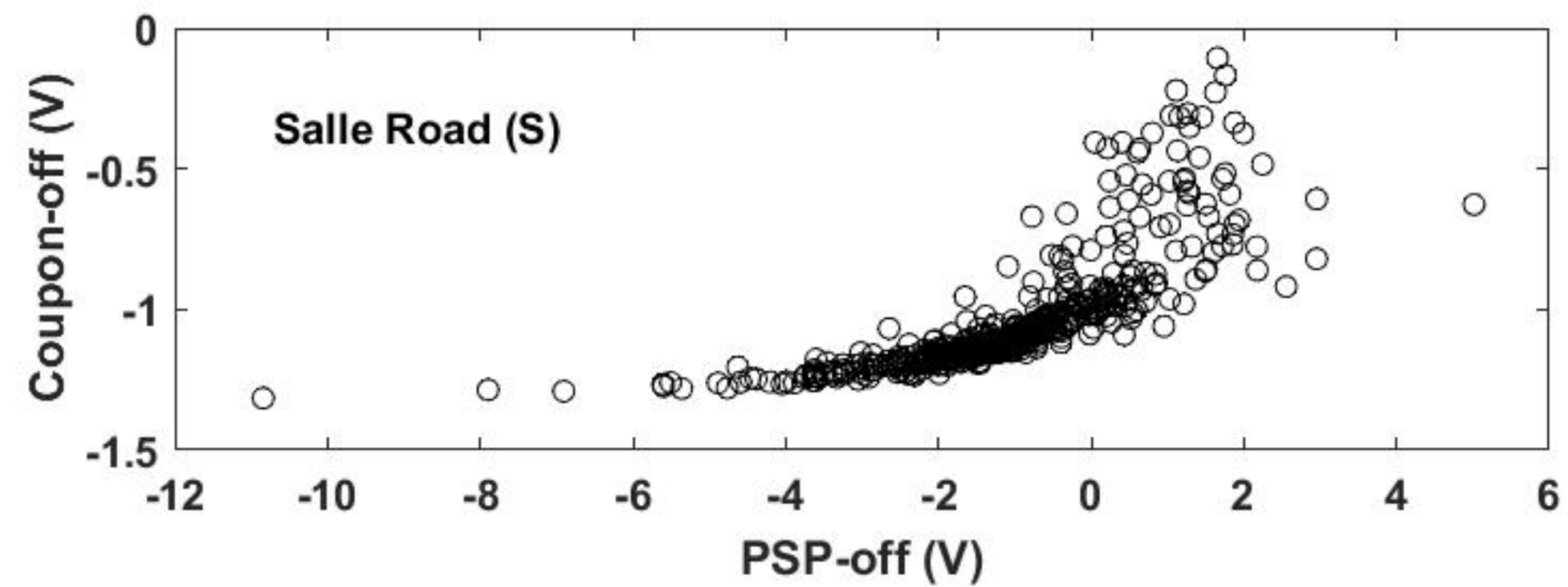


Figure 9.

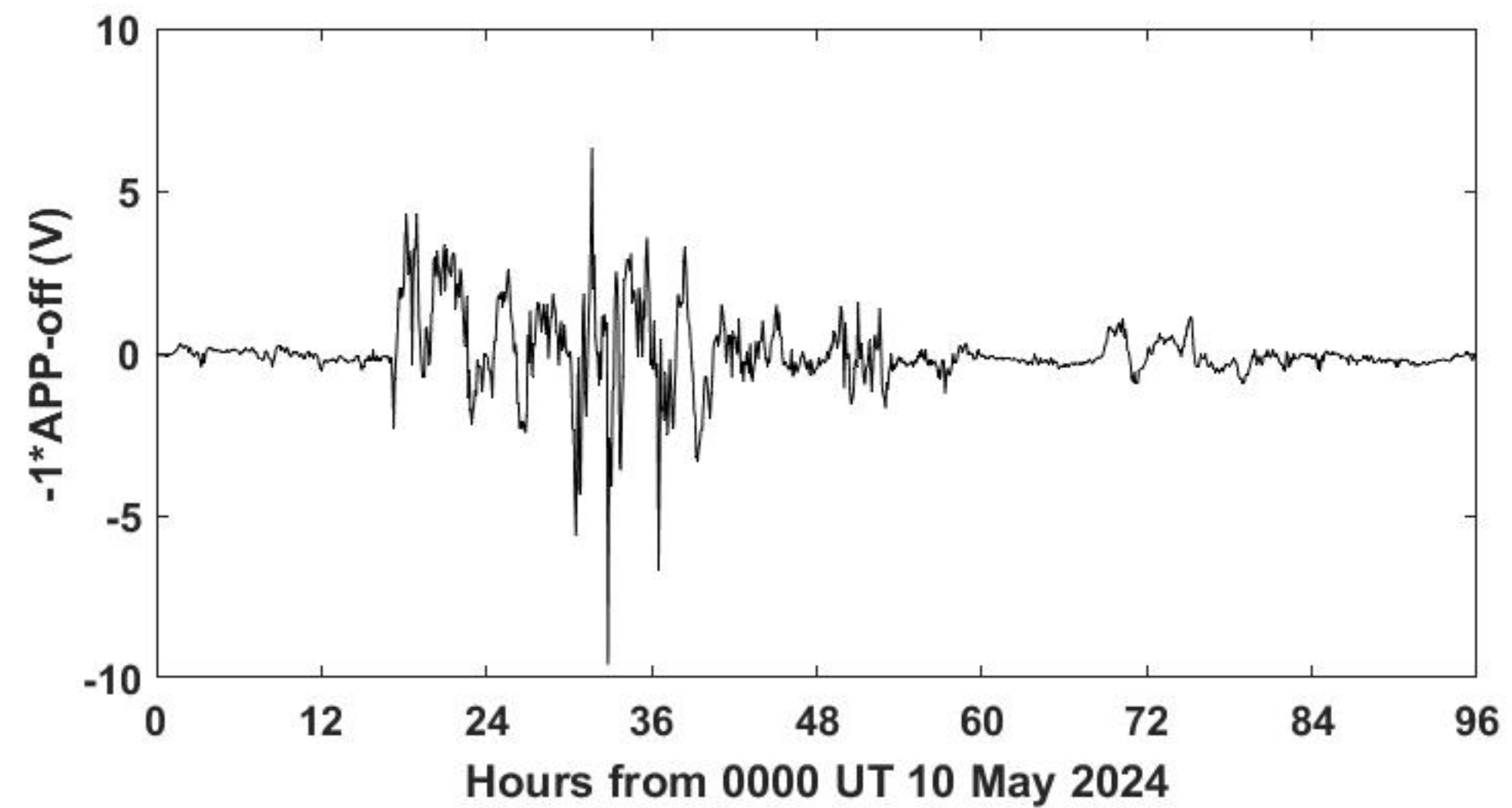
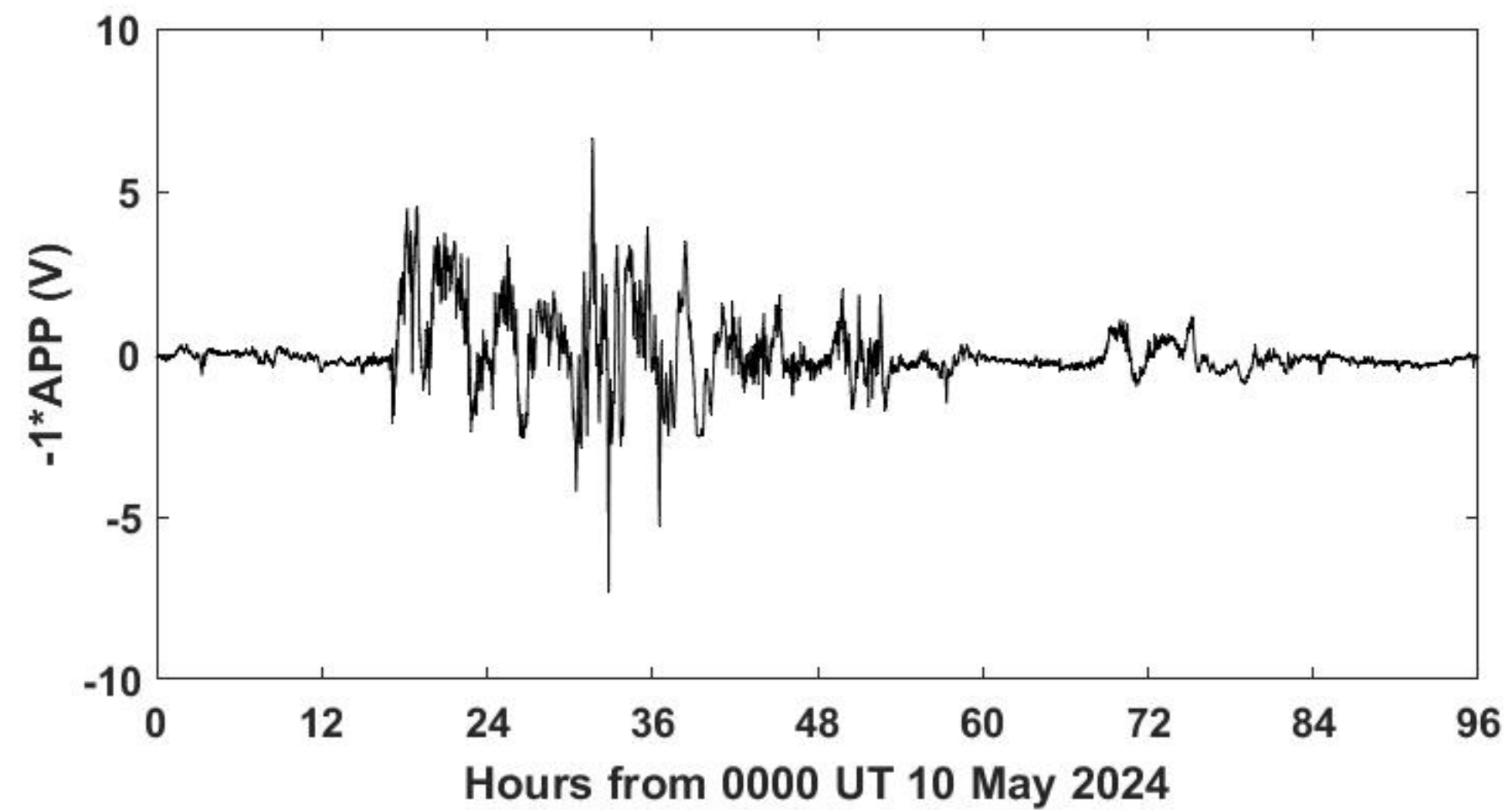
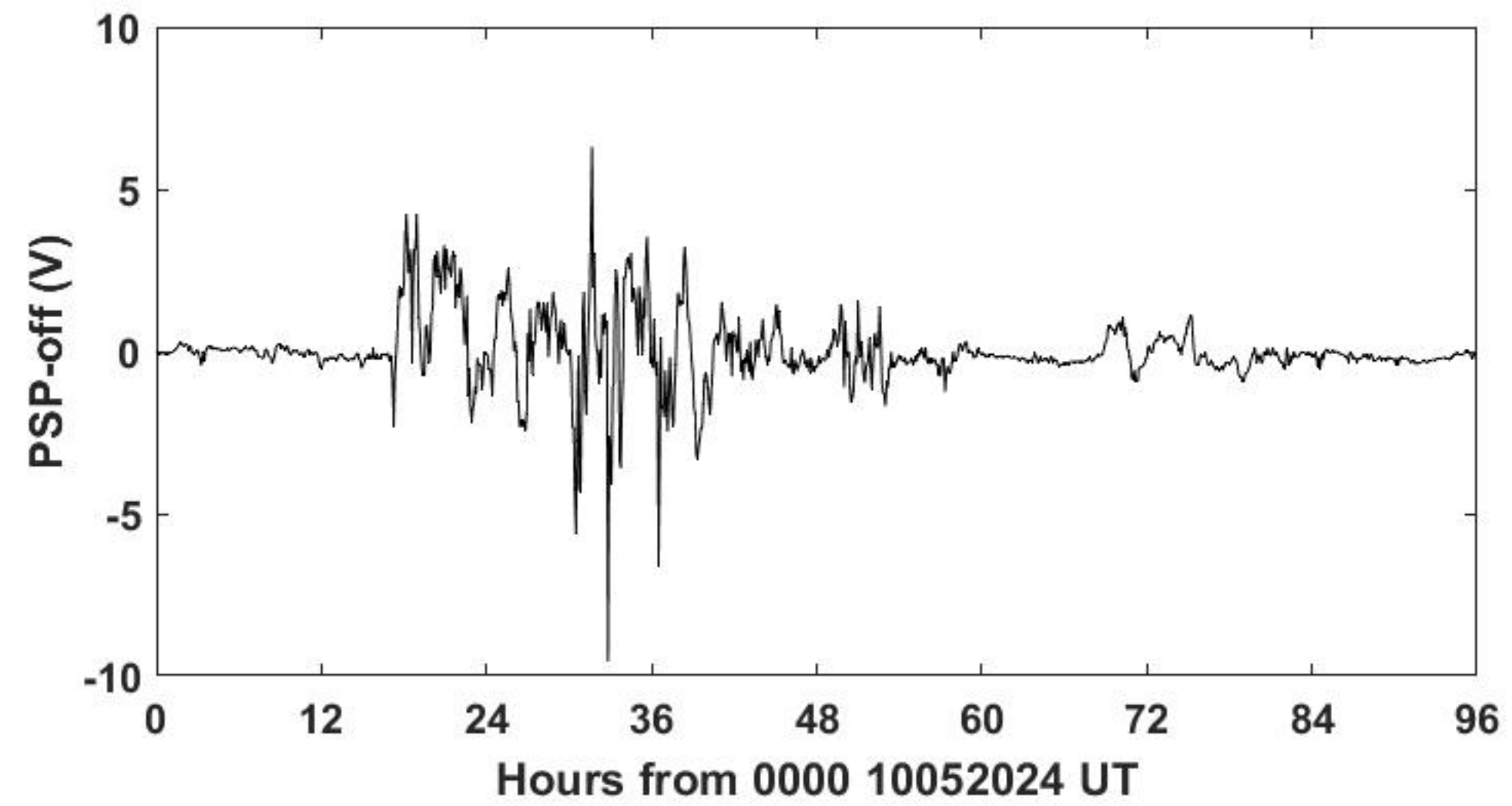
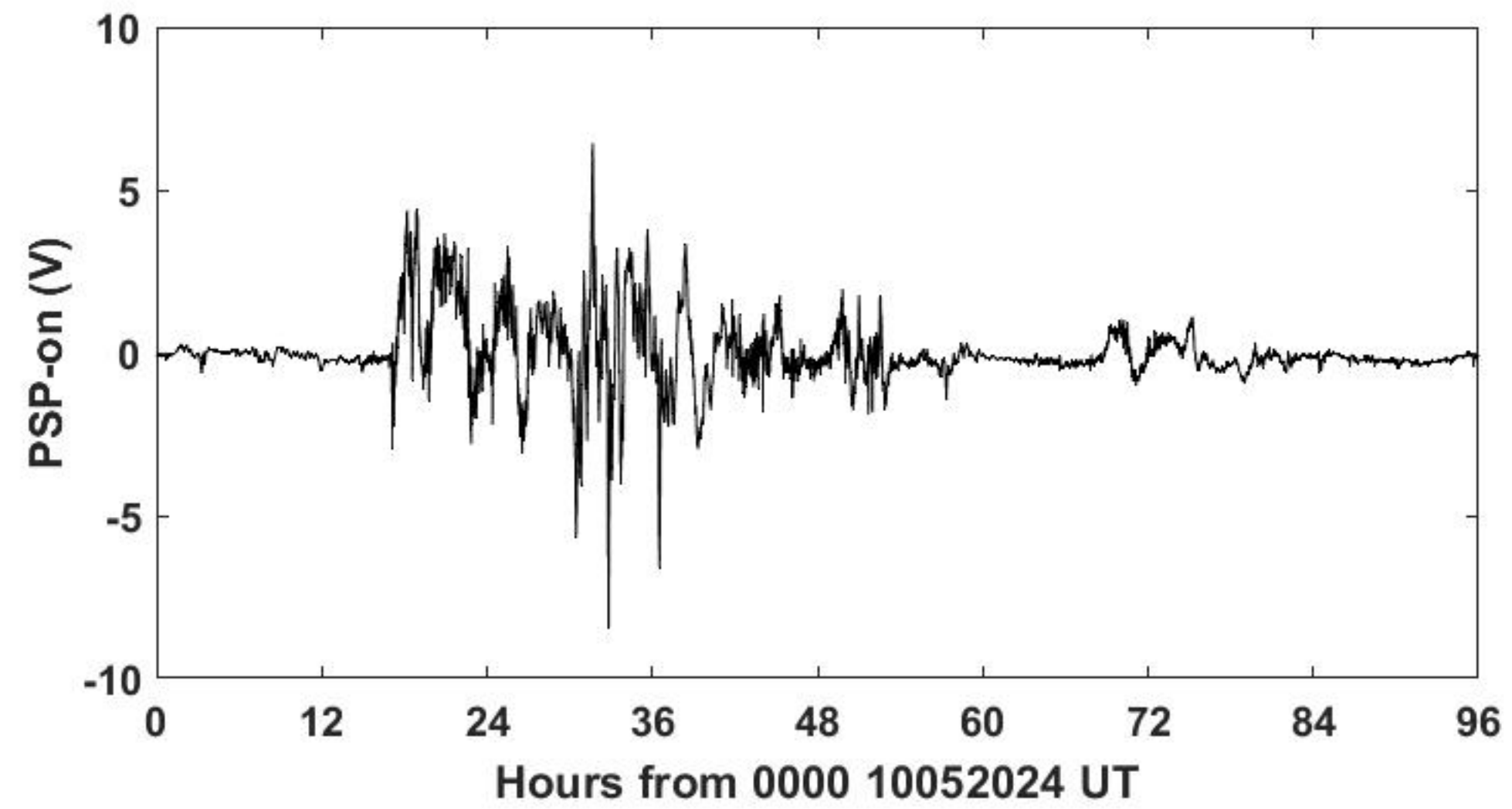


Figure 10.

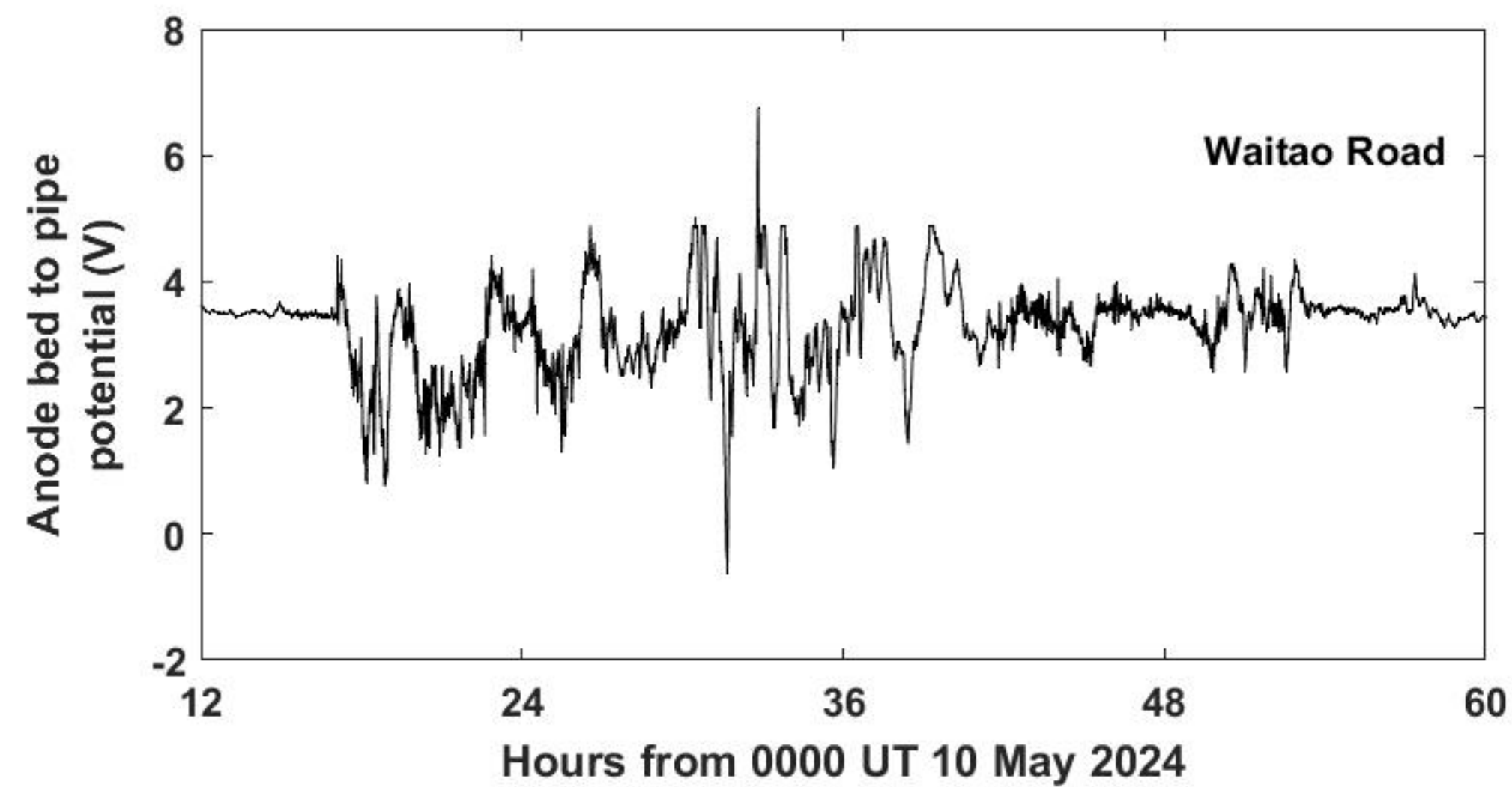
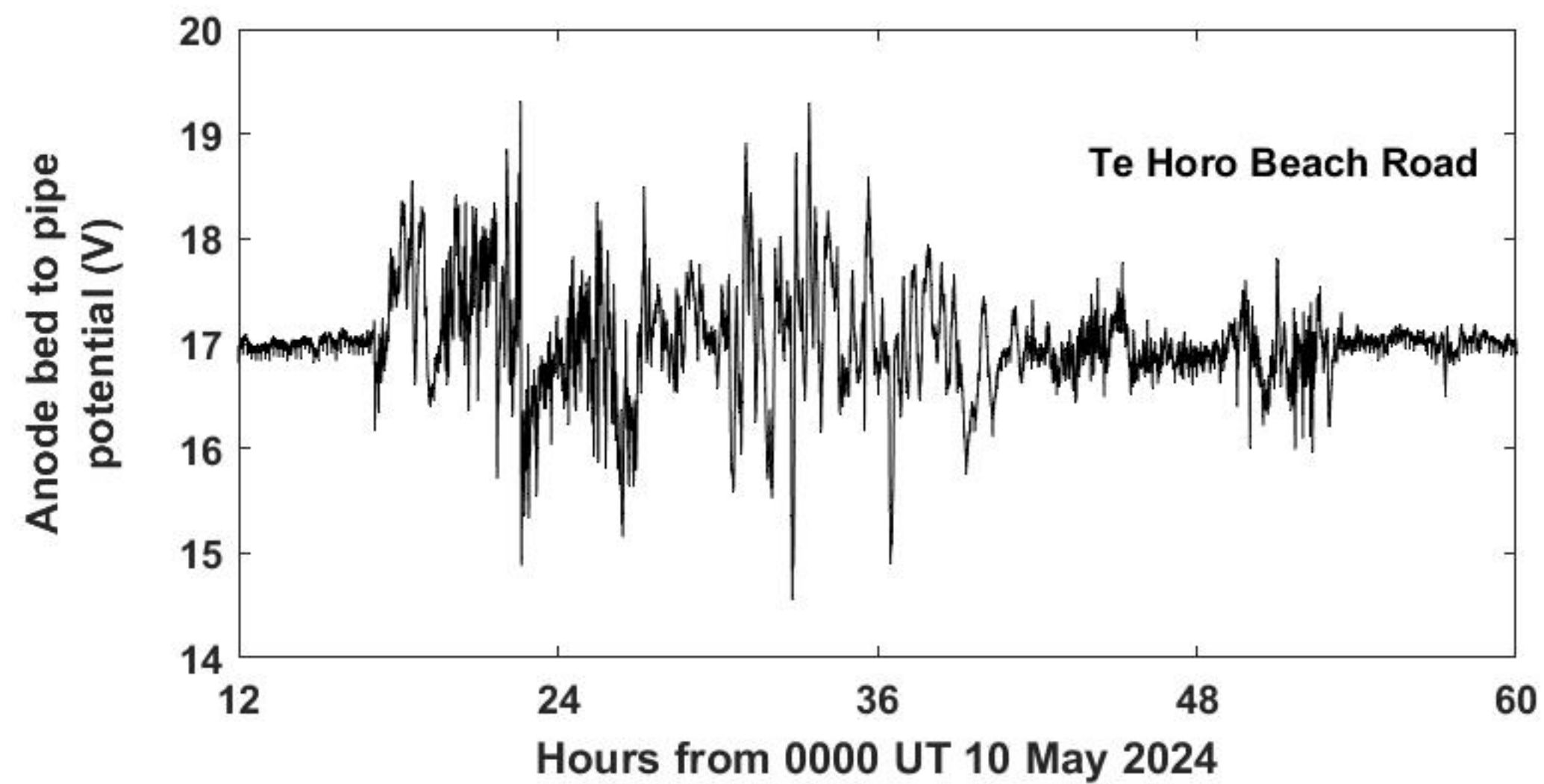
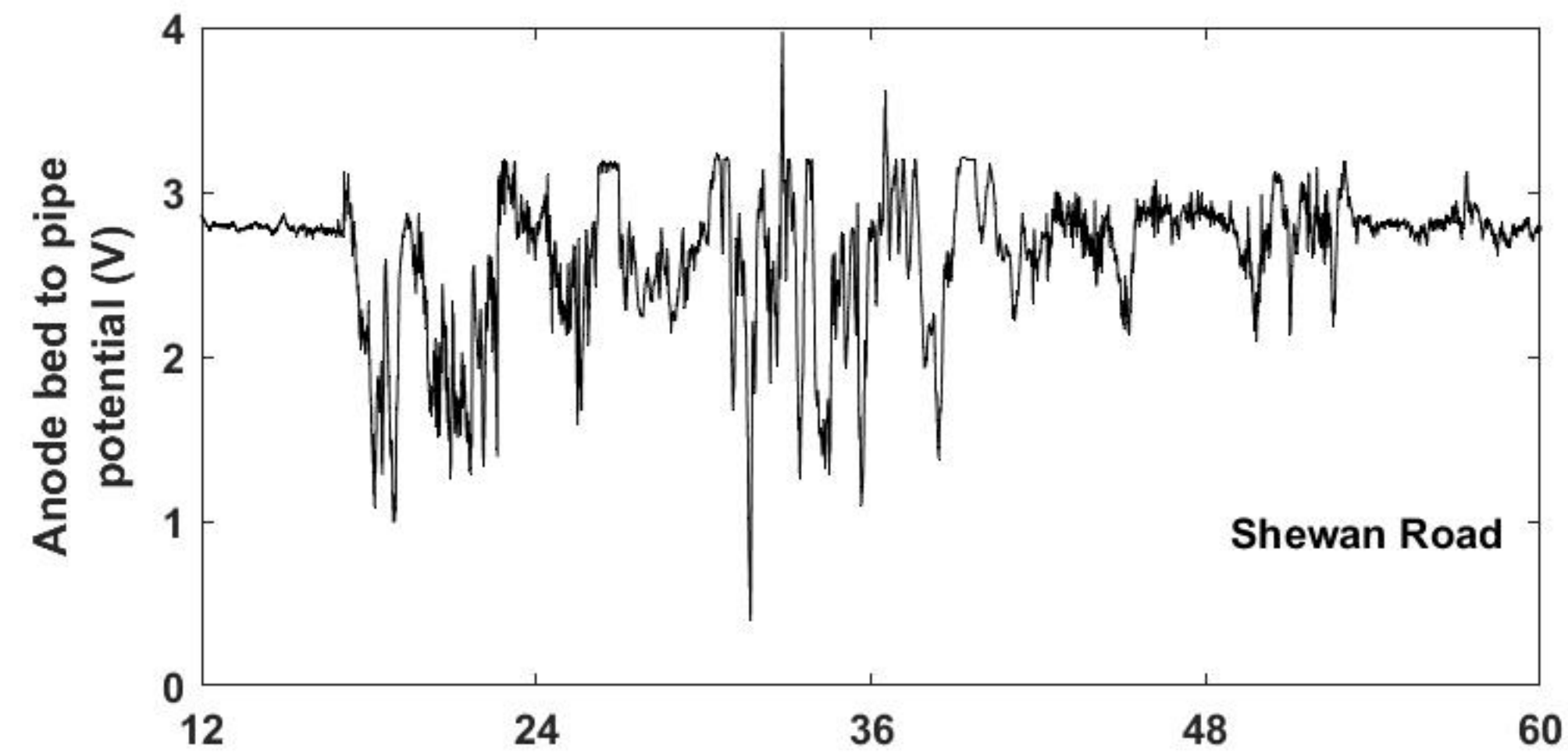
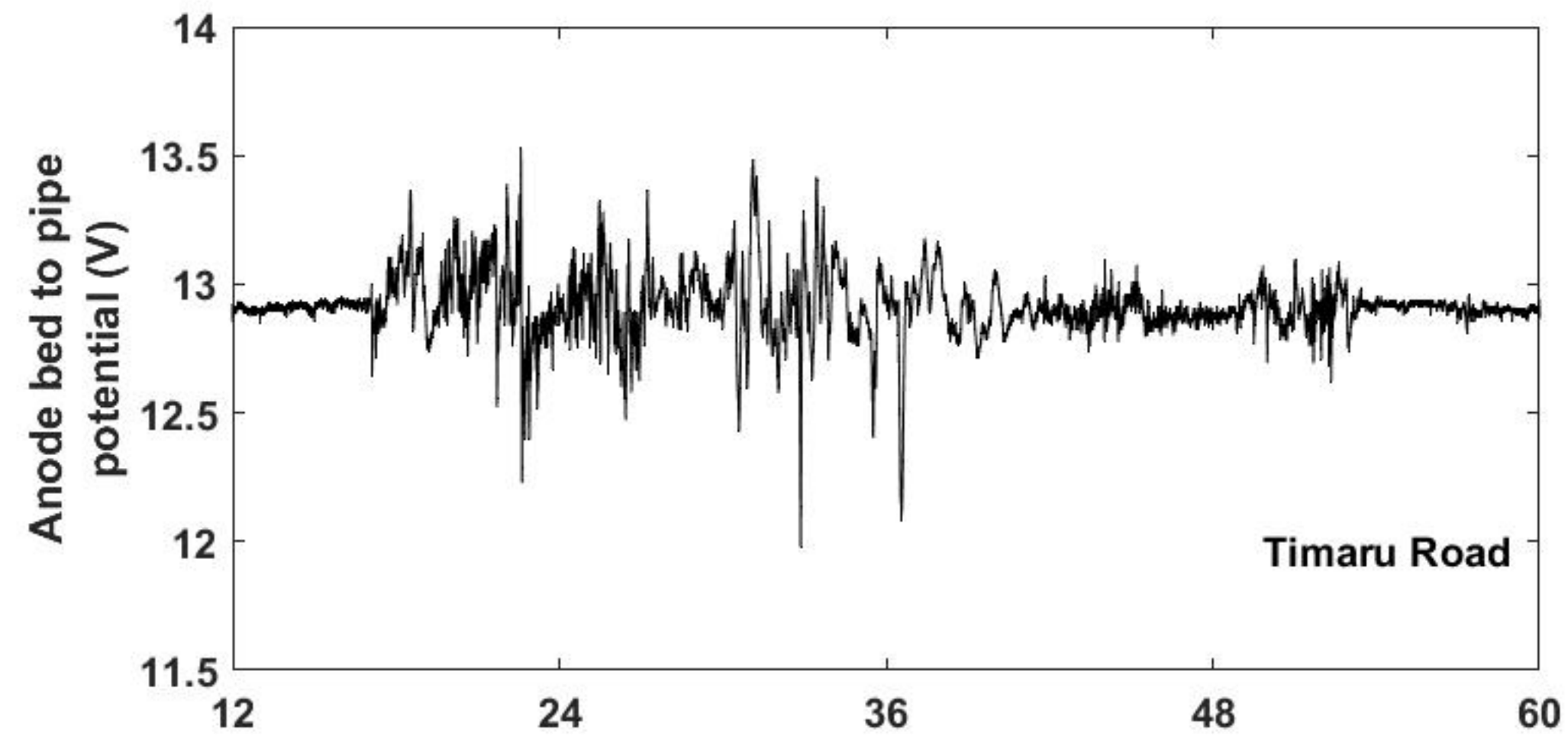


Figure 11.



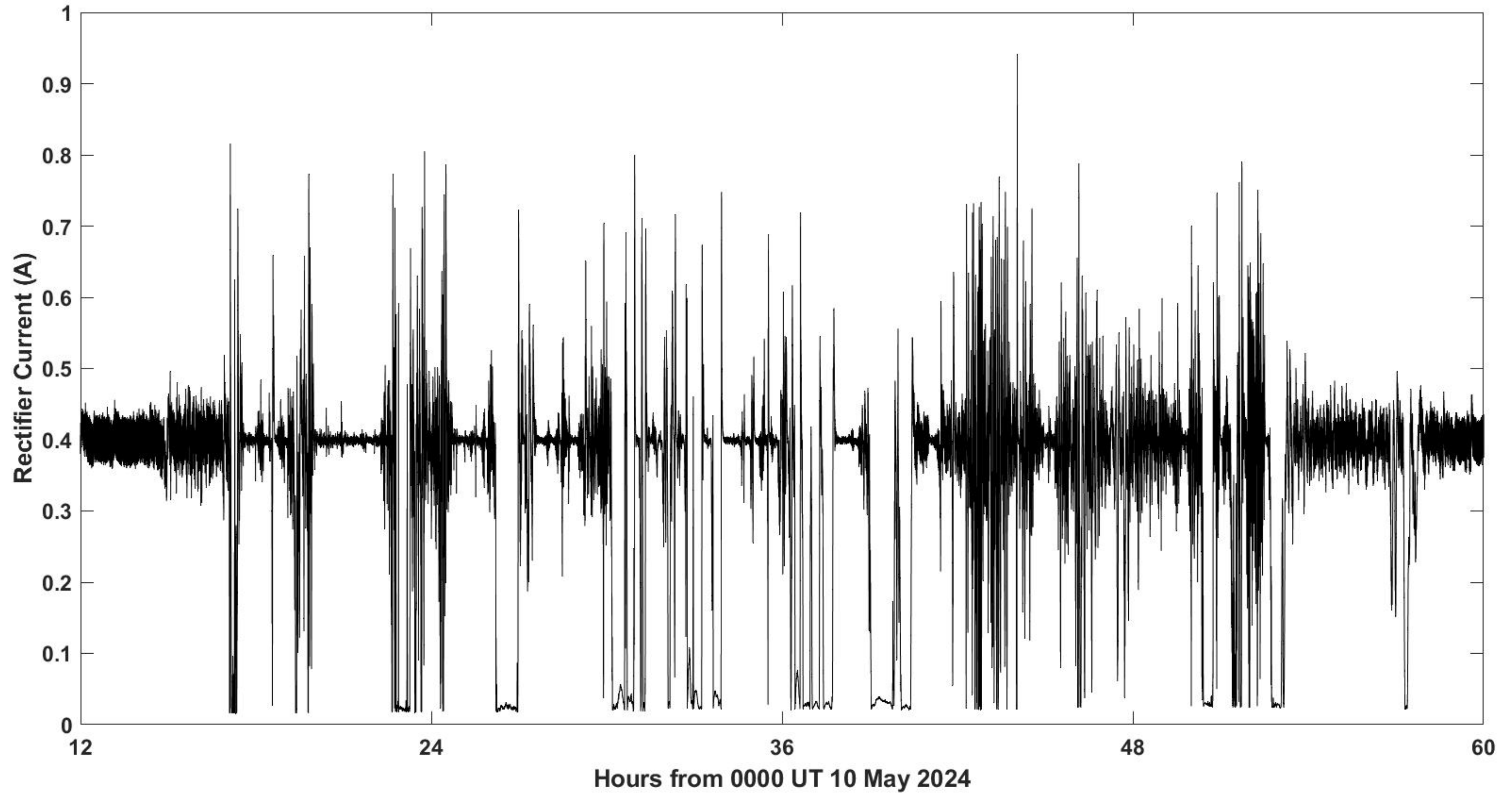


Figure 12.

